

New Features in ALE and SPH in LSDYNA

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Dynamore Forum

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New Features in ALE

Mapping 2D to 3D

1- 2 D Run

```
*SECTION_ALE2D
```

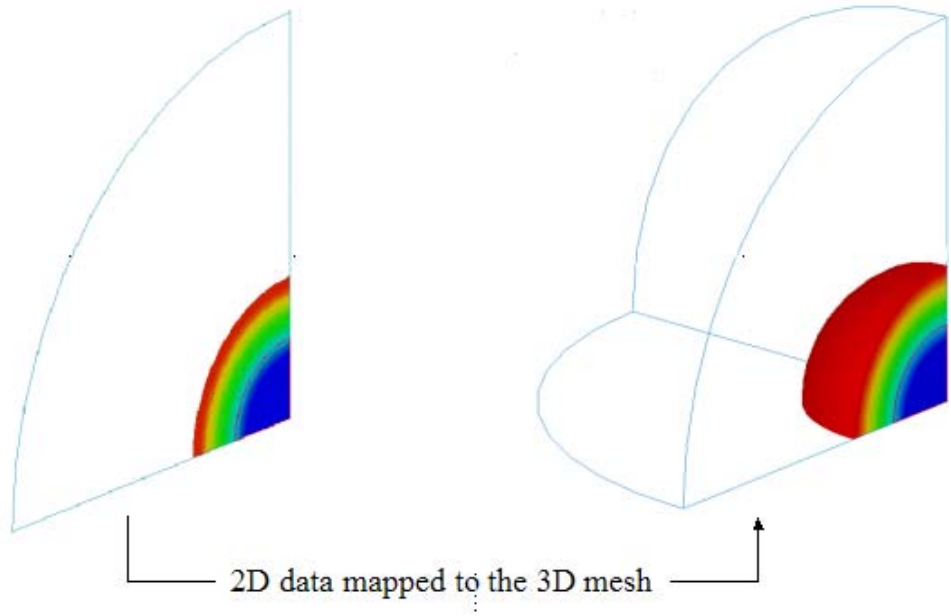
```
ls971 i= input.2d.k  map=filename
```

2- 3 D Run

```
*INITIAL_ALE_MAPPING
```

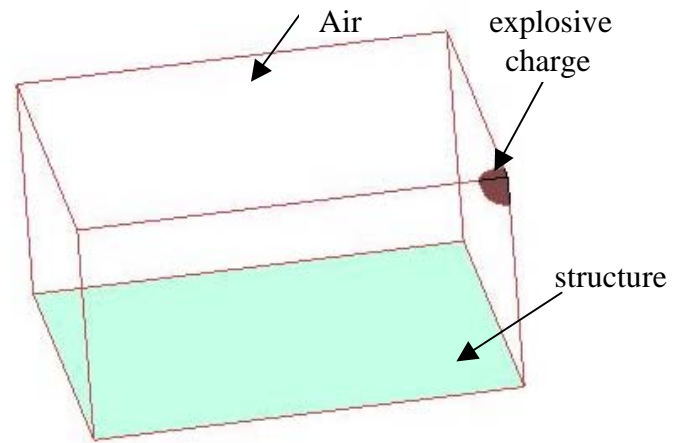
```
$ PartId      Part_Set      AMMG  
      100          0          200
```

```
ls971 i= input.3d.k  map=filename
```





Experimental setup (Boyd 2000)



Numerical model 1.2 Million elements

ALEFSI LINK

Useful for design using multiple ALE runs

```
*DATABASE_BINARY_FSLINK
```

```
1.e-4
```

```
*CONSTRAINED_LAGRANGE_IN_SOLID_TITLE
```

```
$# coupid
```

```
100
```

```
$# slave master sstyp mstyp nquad ctype direc mcoup  
3 5 1 0 0 4
```

```
$# start end pfac fric frcmin norm normtyp damp
```

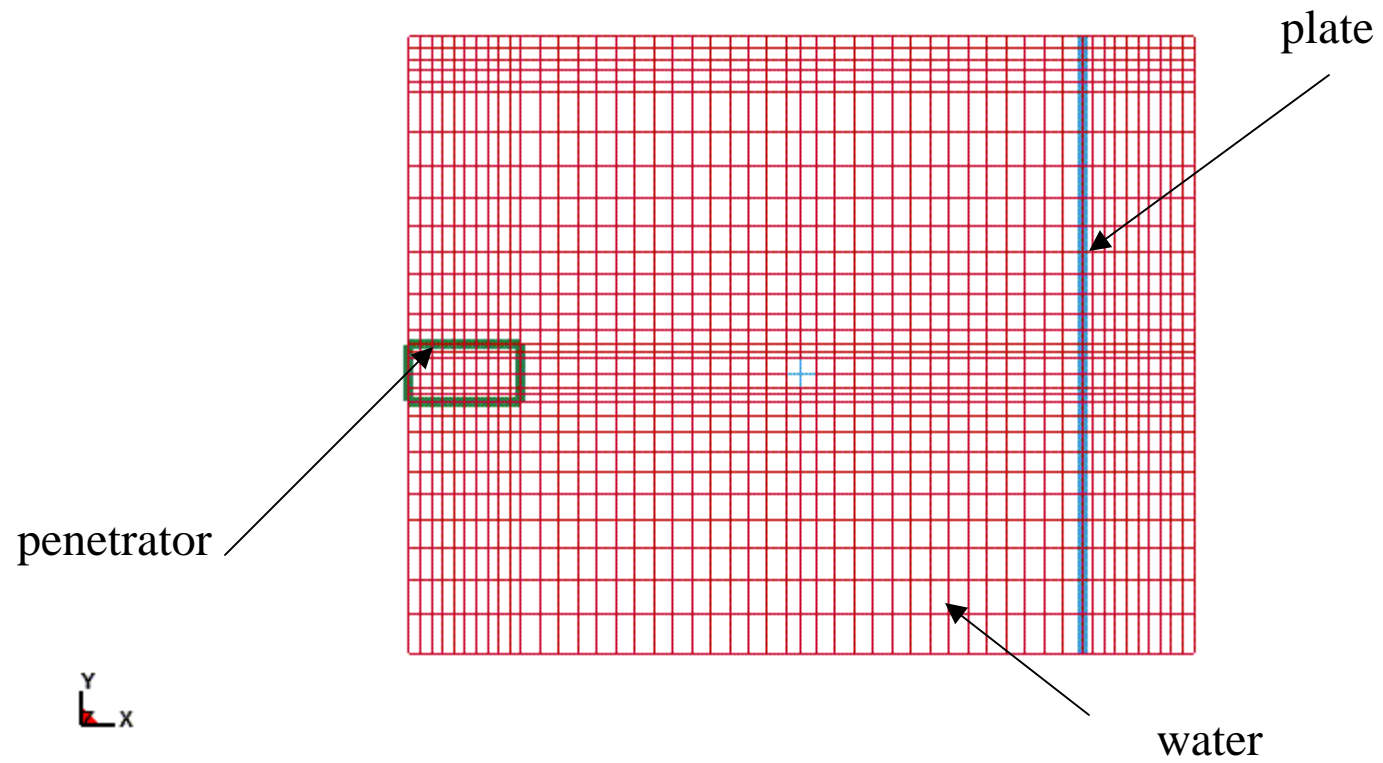
```
$# cq hmin hmax ileak pleak lcidpor nvent blockage
```

```
$# iboxid ipenchk intforc ialesoft lagmul  
0 0 1
```

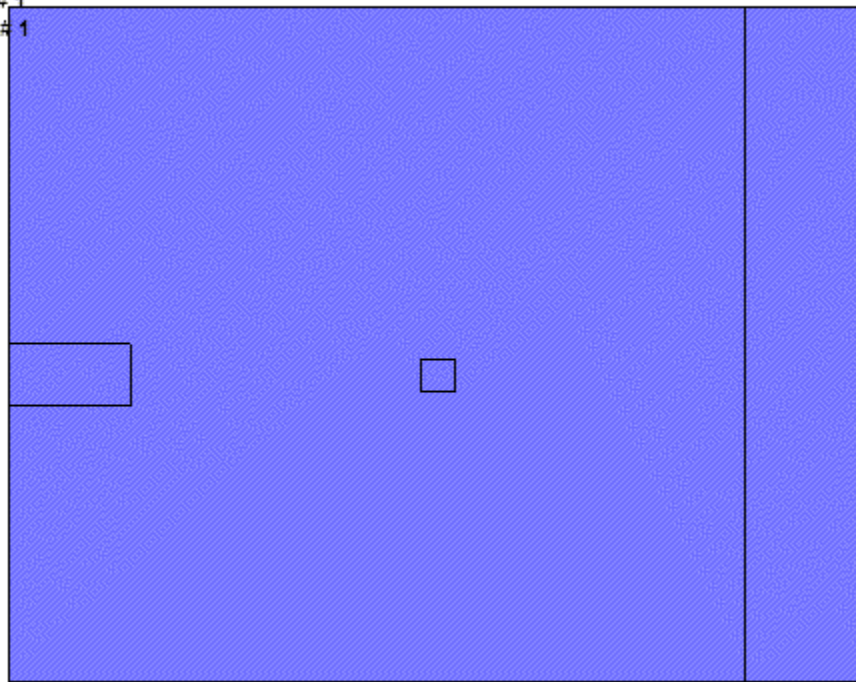
```
ls971 i= input1.k fsilnk=filename
```

Changing the design of the plate

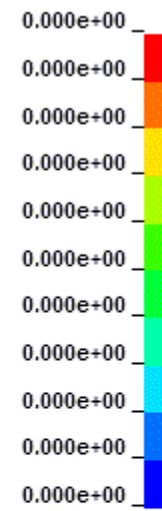
Time = 0



(HE modeled as water)
Time = 0
Contours of Pressure
max ipt. value
min=0, at elem# 1
max=0, at elem# 1



Fringe Levels



ALEFSI LINK

2) Delete all ALE elements from input1.k

Add the following keyword

***LOAD_SEGMENT_FSILINK**

filename

\$ number of interface

1

\$ which interface

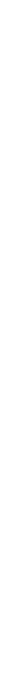
100

run ls971 i=input2.k

Time = 0



(HE modeled as water)
Time = 0



Coupling ALE to Discrete Elements

Similar to

*CONSTRAINED_LAGRANGE_IN_SOLID (constrained coupling)

*ALE_COUPLING_NODAL

```
$# slave master sstyp mstyp ctype mcoup
      3      2      1      1      1      -1
$# start end
   0.000 0.000
```

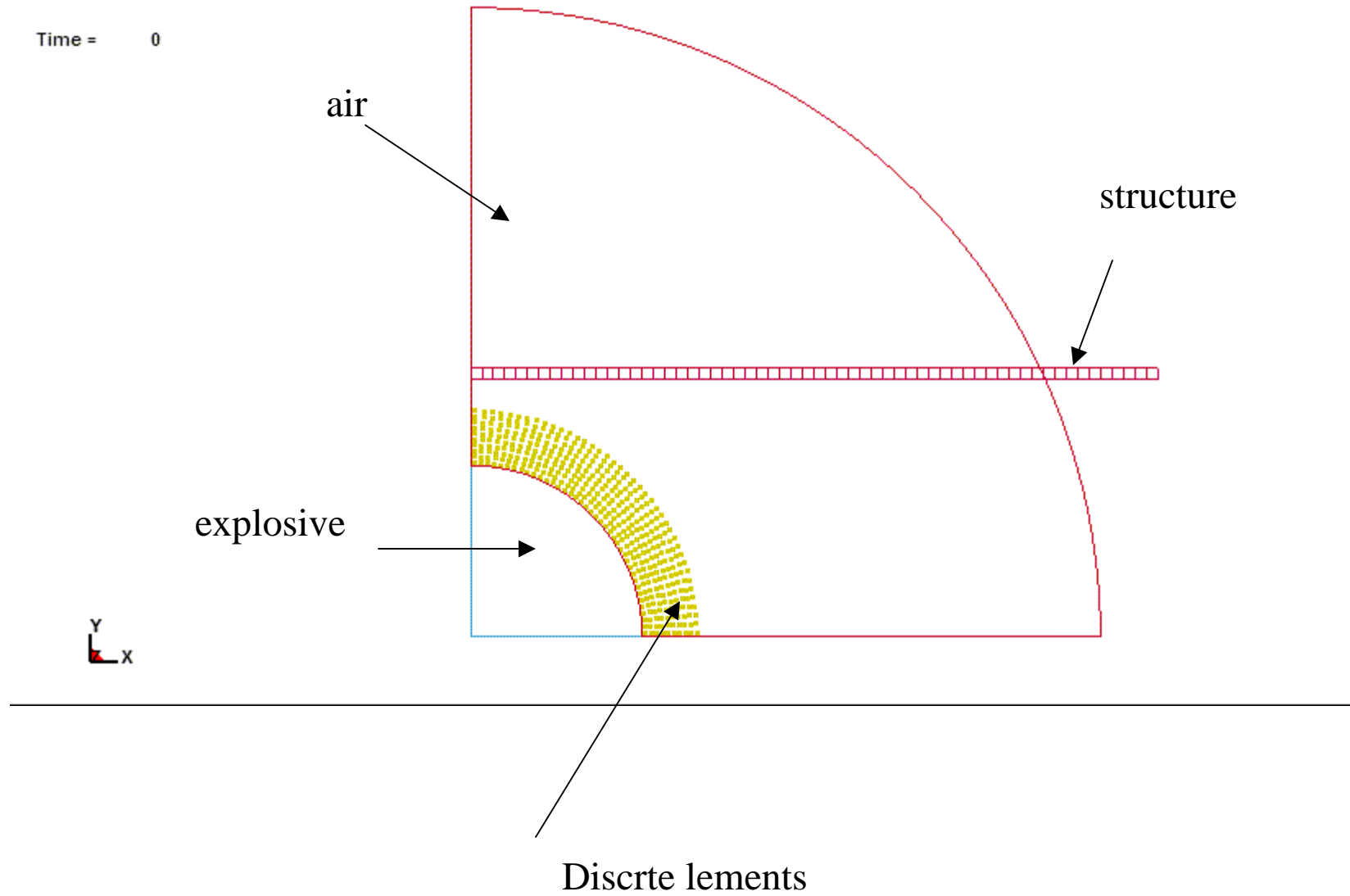
Part 3 discrete elements Part : Slave

Part 2 ALE Part : Master

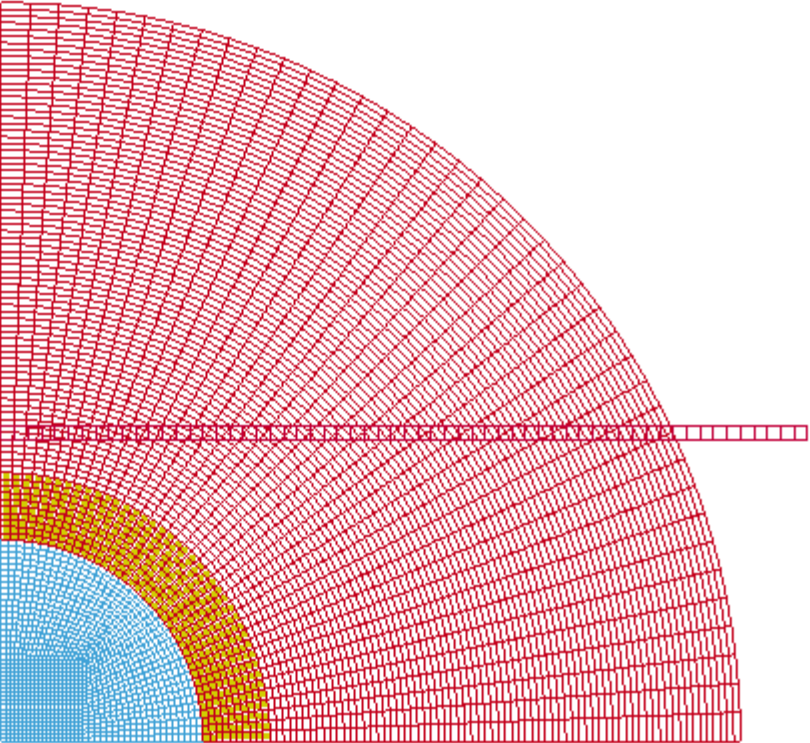
*ELEMENT_DISCRETE_SPHERE

```
$# nid pid mass inertia radius
```

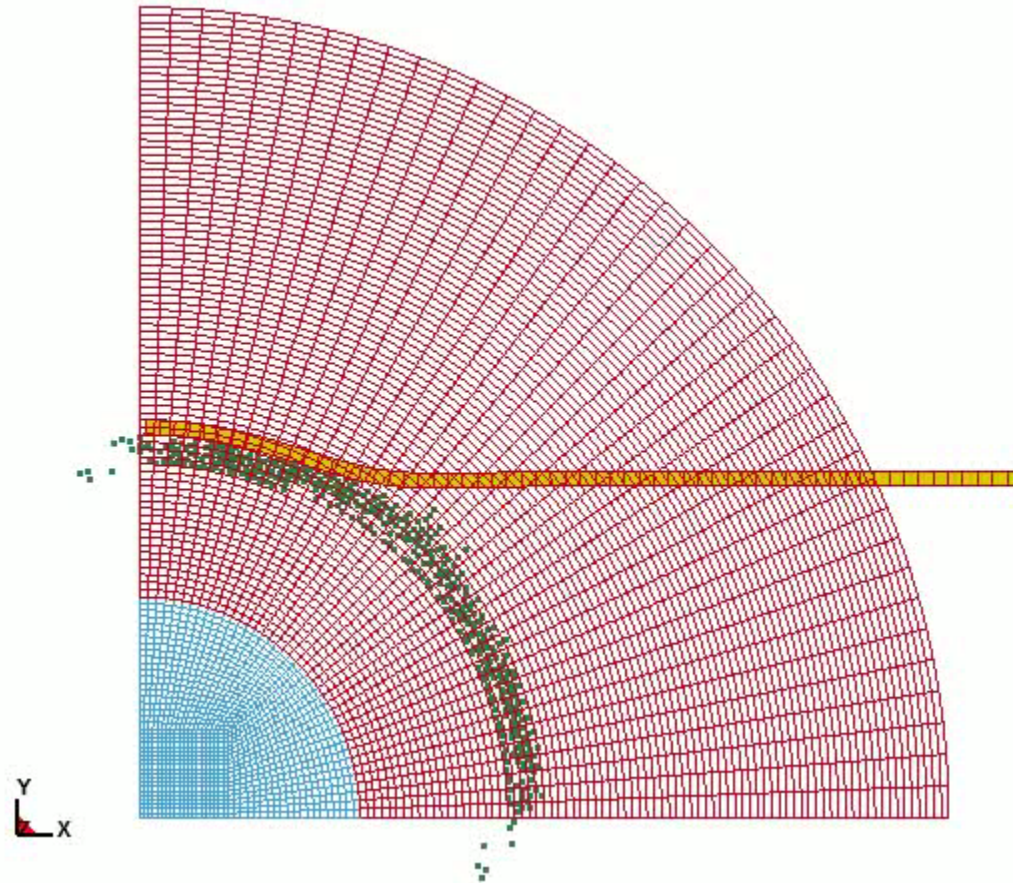
Time = 0



Time = 0



Time = 150.01



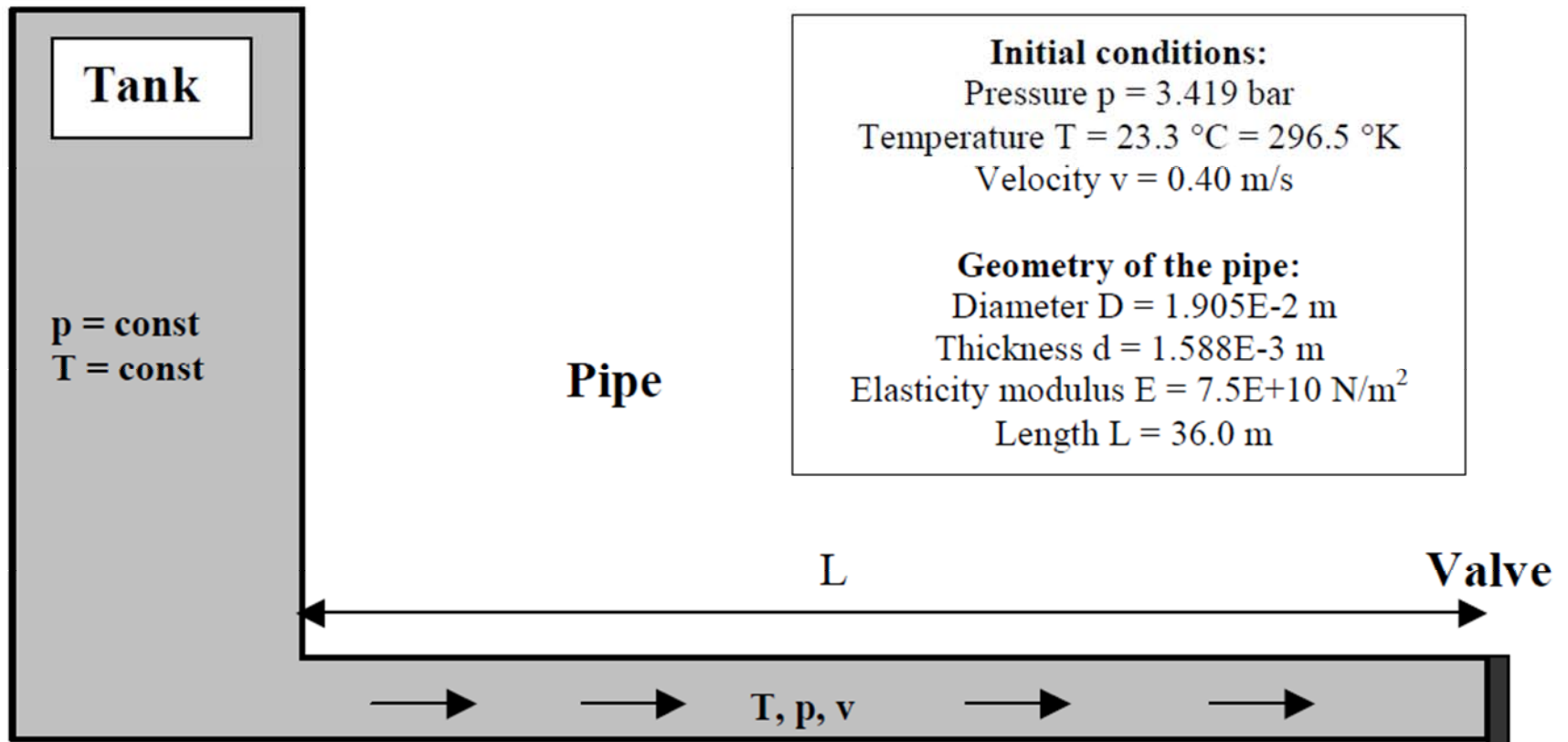
EOS Phase change

*EOS_PHASE_CHANGE

\$	eosid	rho_liq	rho_gas	sp_liq	sp_gas	amb_pres	v0
	1	997.	2.095e-2	1492.00	425.00	1.e+5	0.0000

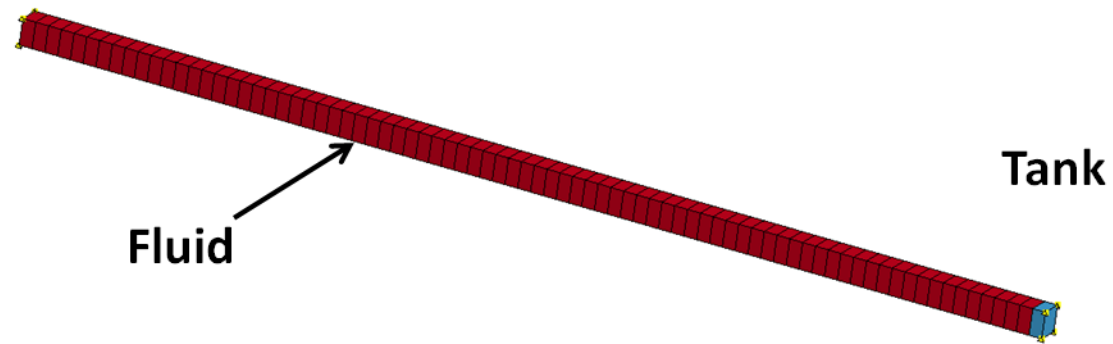
*INITIAL_VAPOR_PART

1



1D WATER HAMMER.

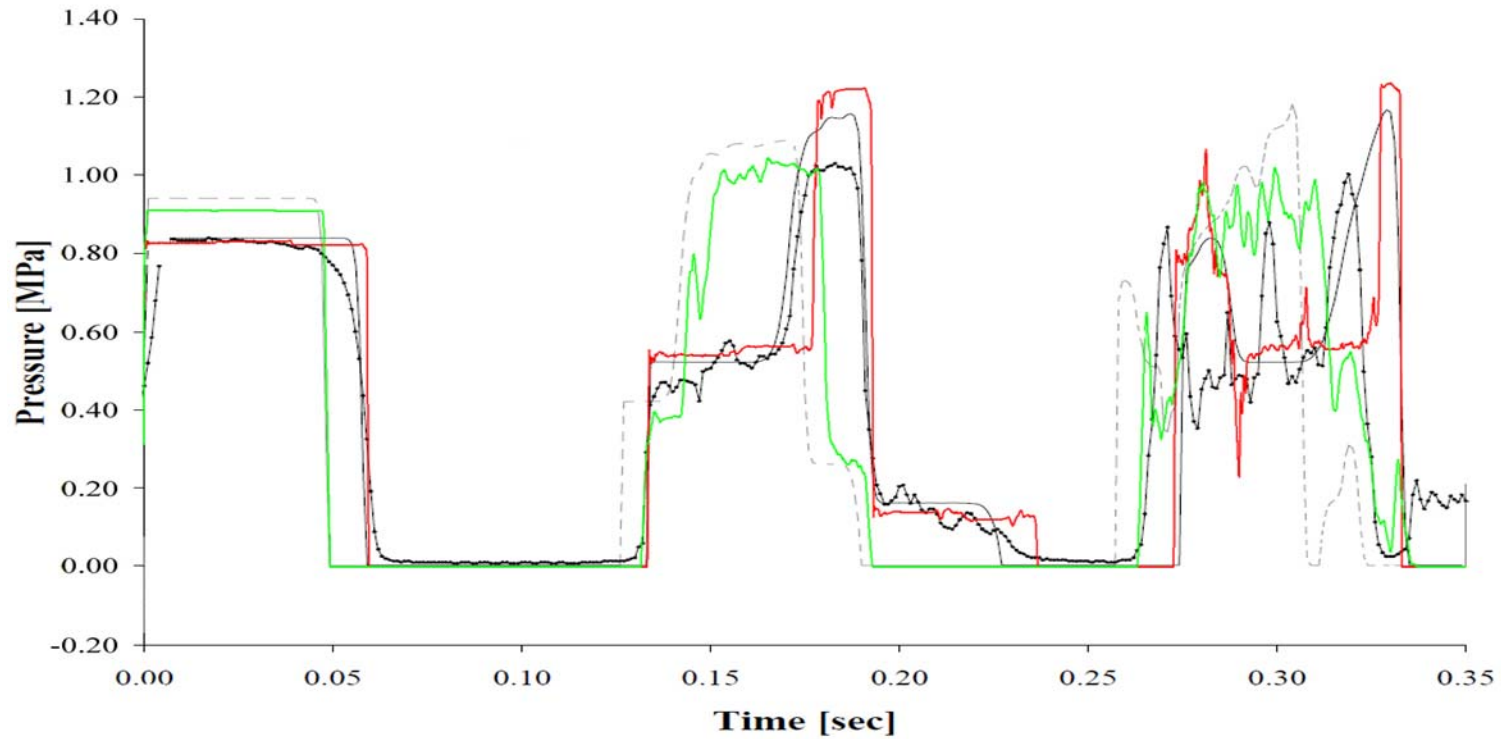
Closed Valve



Tank

- The simulation starts at the closure of the valve ($t=0$).
- All nodes at the closed valve location are fixed (velocity = 0) .
- All fluid nodes are fixed in Y and Z directions.
- One directional flow, no fluid-structure interaction.

Simpson's Experiment Results.



Experimental simulation.

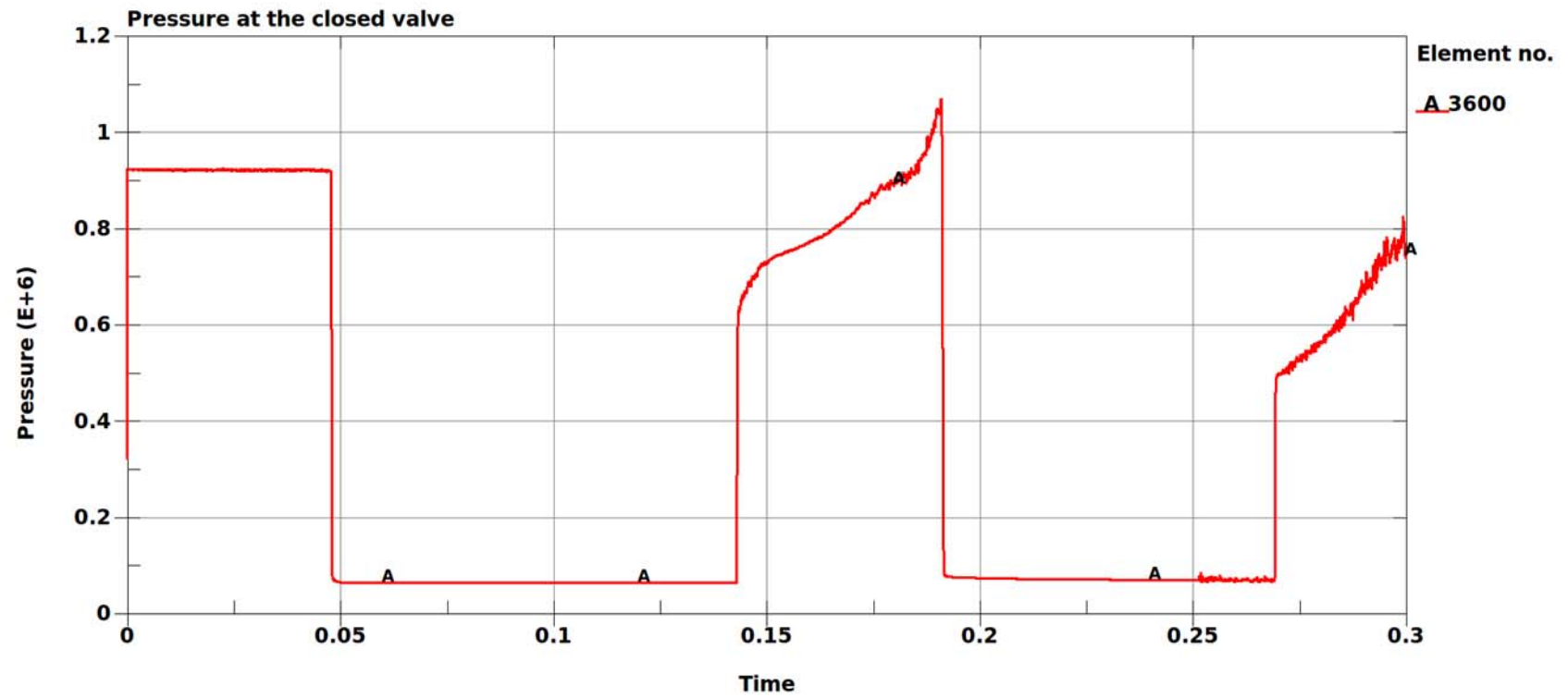
1D simulation.

3D simulation.

Stiff pipe WAHA CODE.

Elastic Pipe WAHA CODE.

PLOT OF PRESSURE AT THE CLOSED VALVE

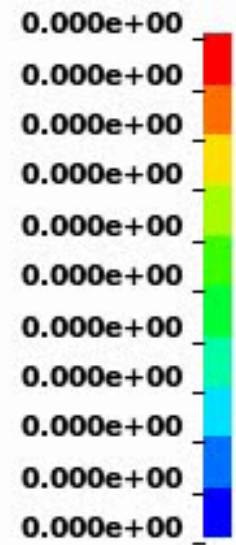


Vapor Volume fraction

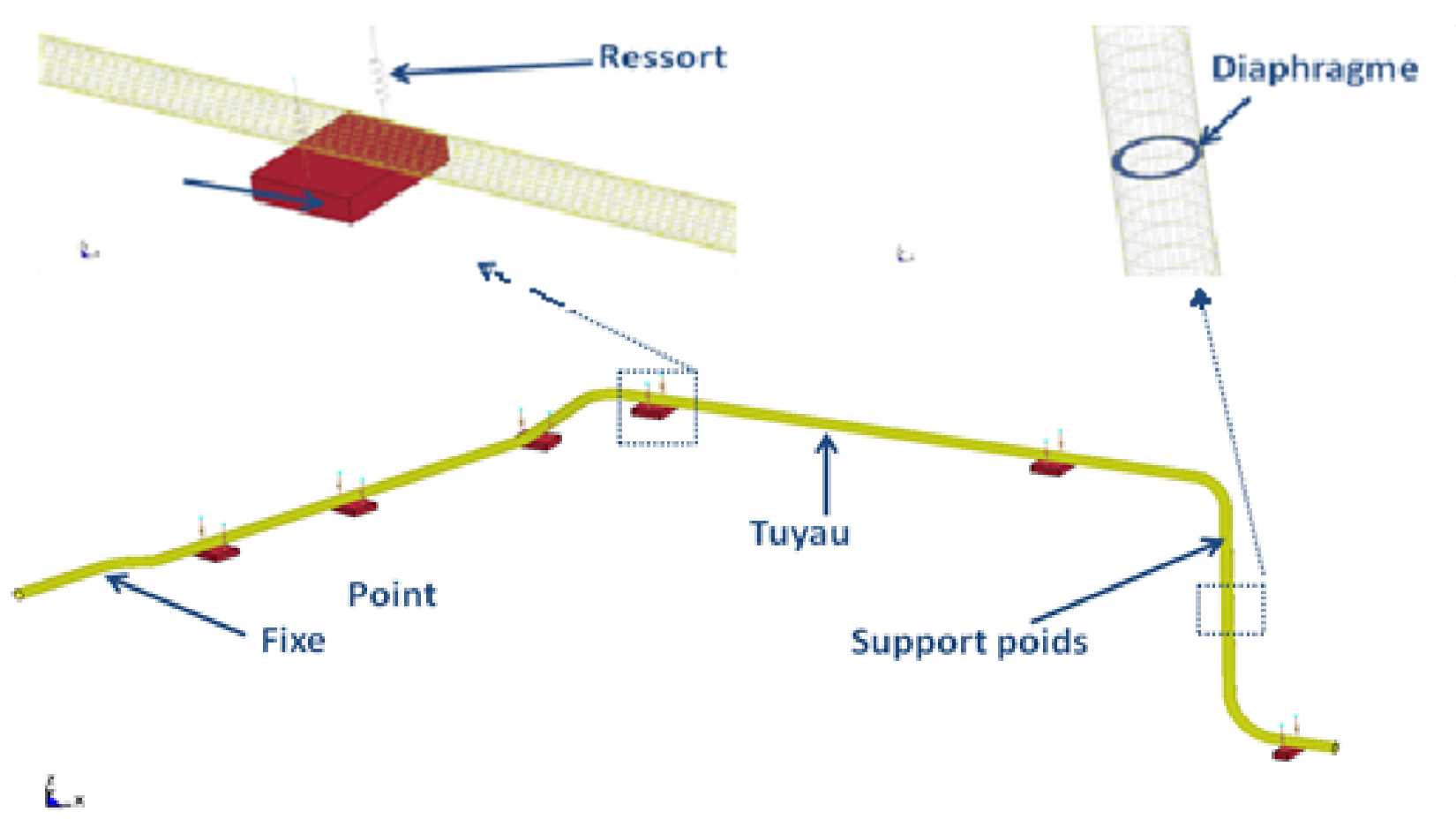
Time = 0



Fringe Levels



EOS Phase change



ALE essential Boundary

*ALE_ESSENTIAL_BOUNDARY

\$#	id	idtype	ictype	iexcl
	1	2	2	0

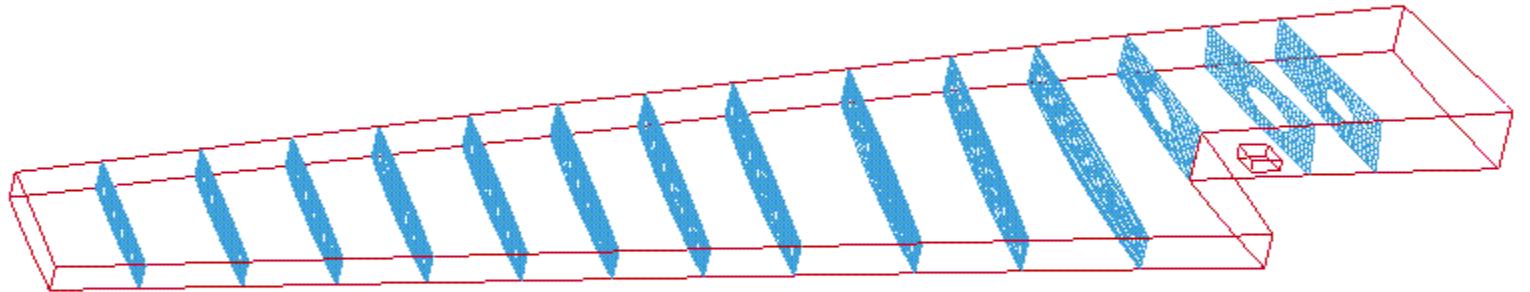
ICTYPE: Constraint type:

EQ.1: No flow through all directions.

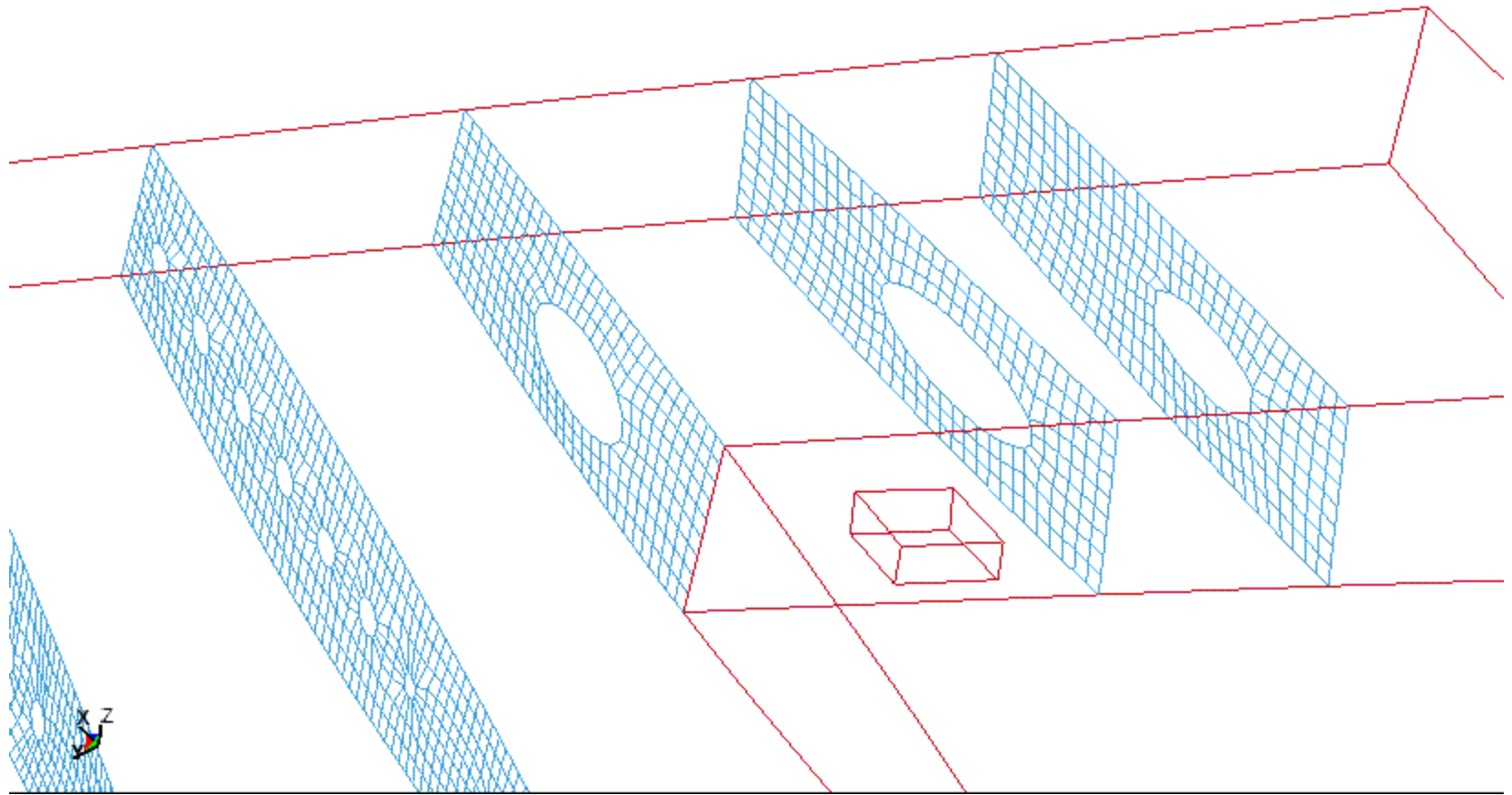
EQ.2: No flow through normal direction. (slip condition)

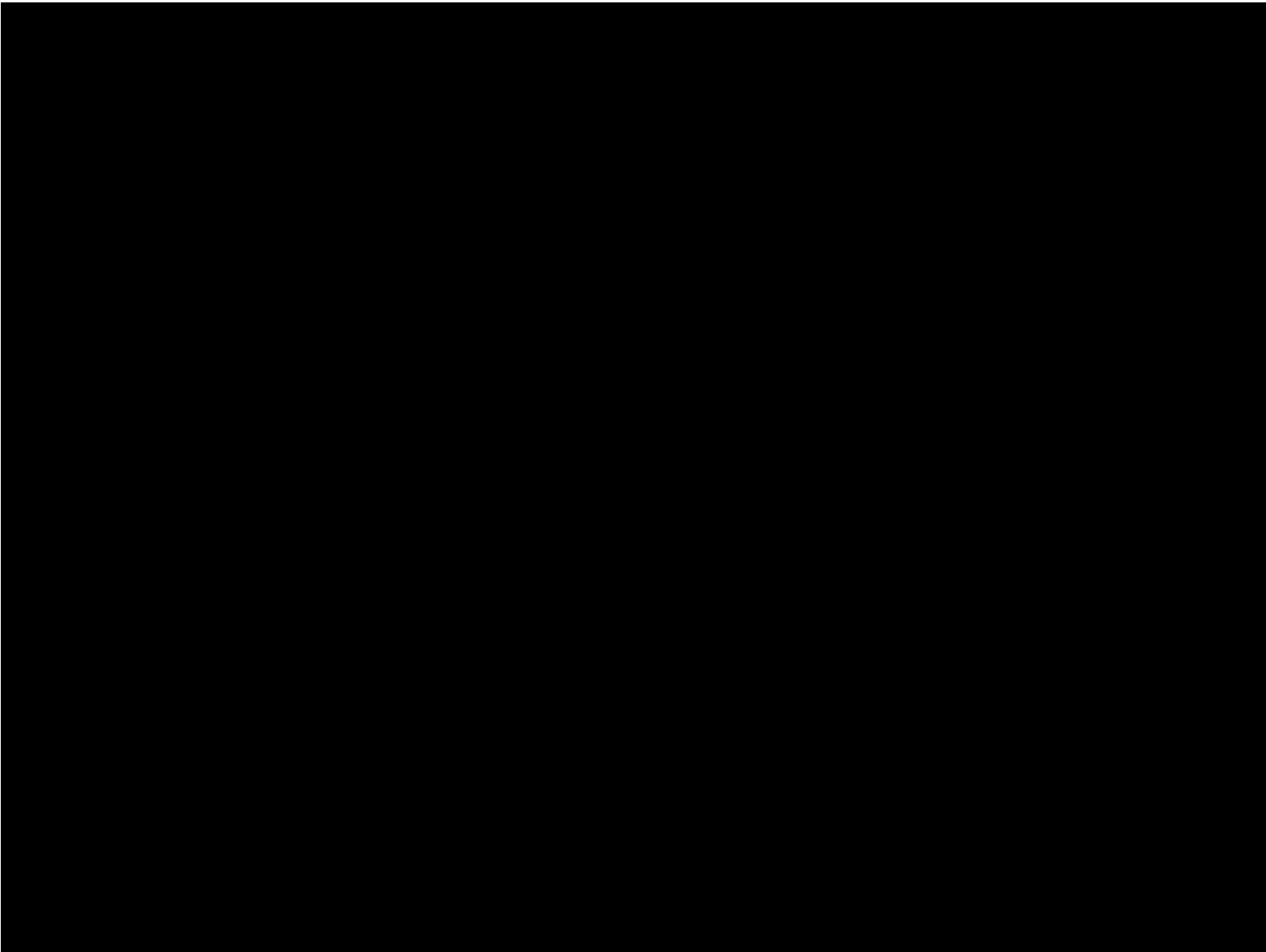
ALE essential Boundary

Filling of airplane tank



ALE essential Boundary





CONTACT in SPH

3D Contact

For 3D Lagrangian LSDYNA Contacts are used for SPH

Penalty Based Contact

*CONTACT_AUTOMATIC_NODES_TO_SURFACE

*CONTACT_NODES_TO_SURFACE

Constrained Based Contact

*CONTACT_TIED_NODES_TO_SURFACE

*CONTACT_TIED_NODES_TO_SURFACE_OFFSET

*CONTACT_CONSTRAINT_NODES_TO_SURFACE

CONTACT in SPH

2D Contact only for SPH

*CONTACT_2D_NODE_TO_SOLID

*CONTACT_2D_NODE_TO_SOLID_TIED

*

New Coupling methods for SPH

*DEFINE_ADAPTIVE_SOLID_TO_SPH

*DEFINE_SPH_TO_SPH_COUPLING

*DEFINE_ADAPTIVE_SOLID_TO_SPH

Variable	IPID	ITYPE	NQ	IPSPH	ISSPH	ICPL	IOPT	
Type								
Default	none	none	none	none	none	0	none	

- **IPID** Solid part ID or part set ID
- **ITYPE** Solid part type:

EQ. 0: IPID is part ID

EQ. 1: IPID is part set ID

- **NQ** Refinement option:

EQ. 1: Refine 1 solid element into 1 SPH particle

EQ. 2: Refine 1 solid element into 8 SPH particles

EQ. 3: Refine 1 solid element into 27 SPH particles

- **IPSPH** Part ID for newly generated SPH elements

- **ISSPH** Section ID for SPH element

- **ICPL** Coupling with solid element = 0 no coupling to parent solid elements: **debris simulation**

=1 coupling to parent solid elements

- **IOPT** Coupling method = 0 coupling SPH from time $t=0$ (used for **tied contact SOLID to SPH**)

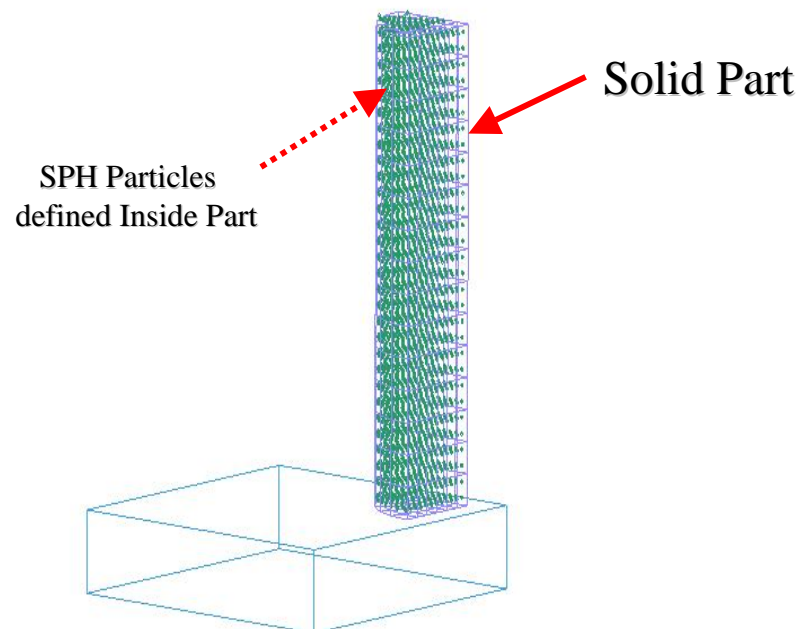
= 1 coupling SPH after failure of solid element

New Contacts in SPH

*DEFINE_ADAPTIVE_SOLID_TO_SPH

After element erosion, we lose the element mass and momentum

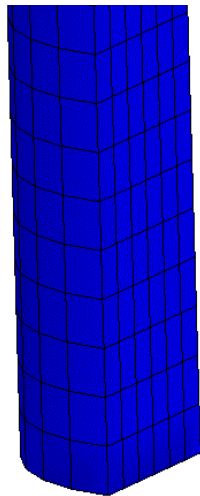
To keep mass and momentum of eroded element, the eroded element is replaced by one or more SPH particles ($NQ > 1$)



*DEFINE_ADAPTIVE_SOLID_TO_SPH

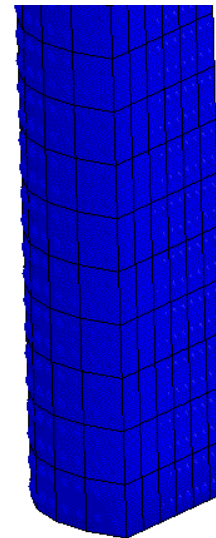
Eroded element are not replaced by particles

Time = 0



Eroded element replaced by particles

Time = 0

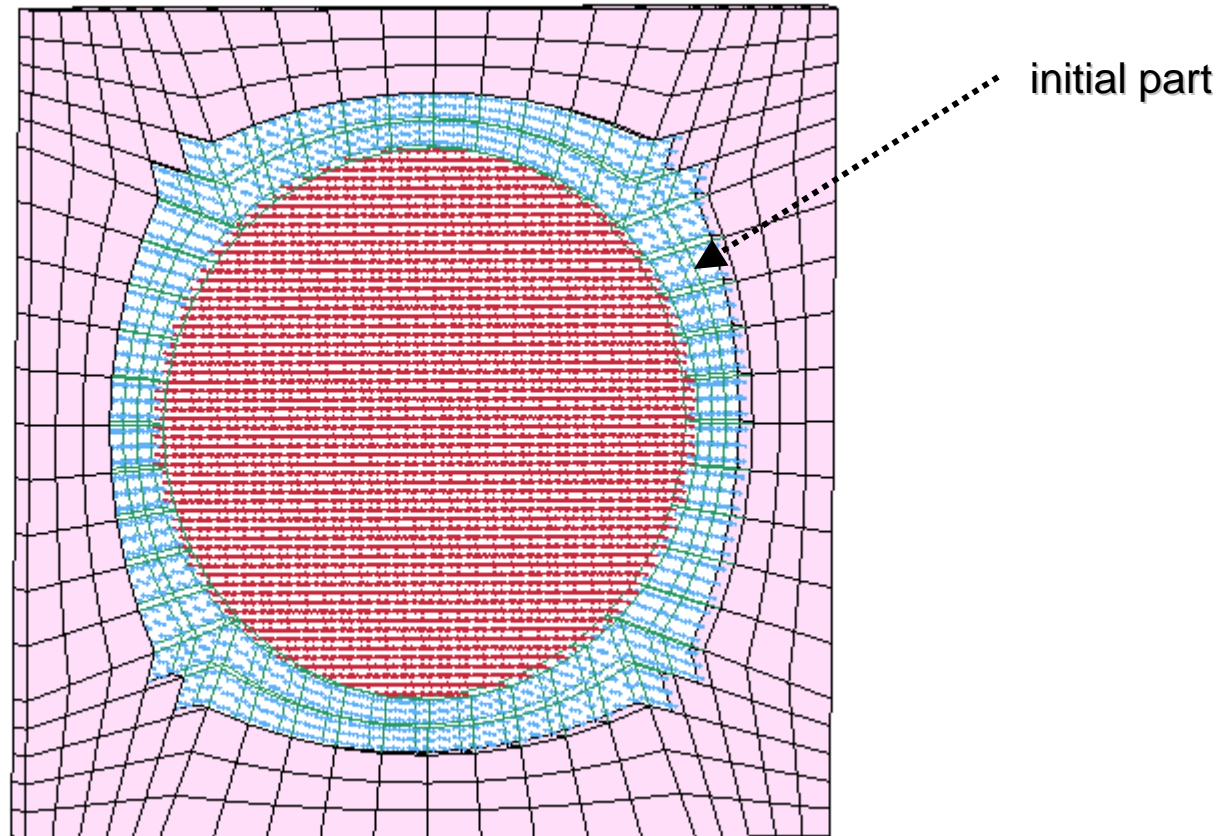


New Contacts in SPH

*DEFINE_ADAPTIVE_SOLID_TO_SPH

ICPL=1 IOPT=0

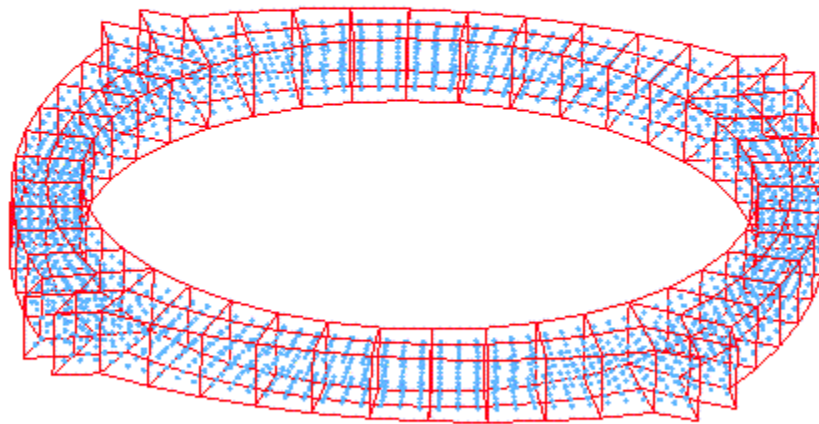
- 1) Particles are active from start to interact with other particle parts (ICPL=1)
- 2) Coupling between particles and the initial part (IOPT=0)



New Contacts in SPH

`*DEFINE_ADAPTIVE_SOLID_TO_SPH`

for tied contact use only **ICPL=1 IOPT=0**

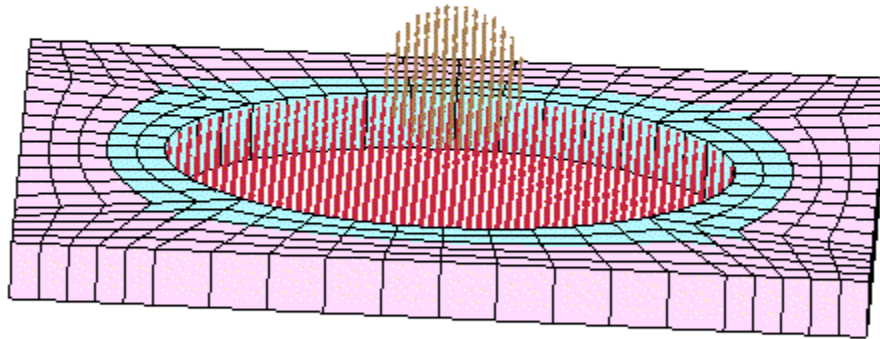


New Contacts in SPH

*DEFINE_ADAPTIVE_SOLID_TO_SPH
ICPL=1

ICPL=1 used only as tied contact between FEM and particles

Generated SPH Particles **are active** from start to interact with other particle parts



New Contacts in SPH

*DEFINE_SPH_TO_SPH_COUPLING

set CONT=1 on *CONTROL_SPH

Variable	SSID	MSID	SSTYPE	MSTYP	IBOX1	IBOX2	PFACT	
Type								
Default	none	none	none	none			1.	

This acts like multi-material in ALE

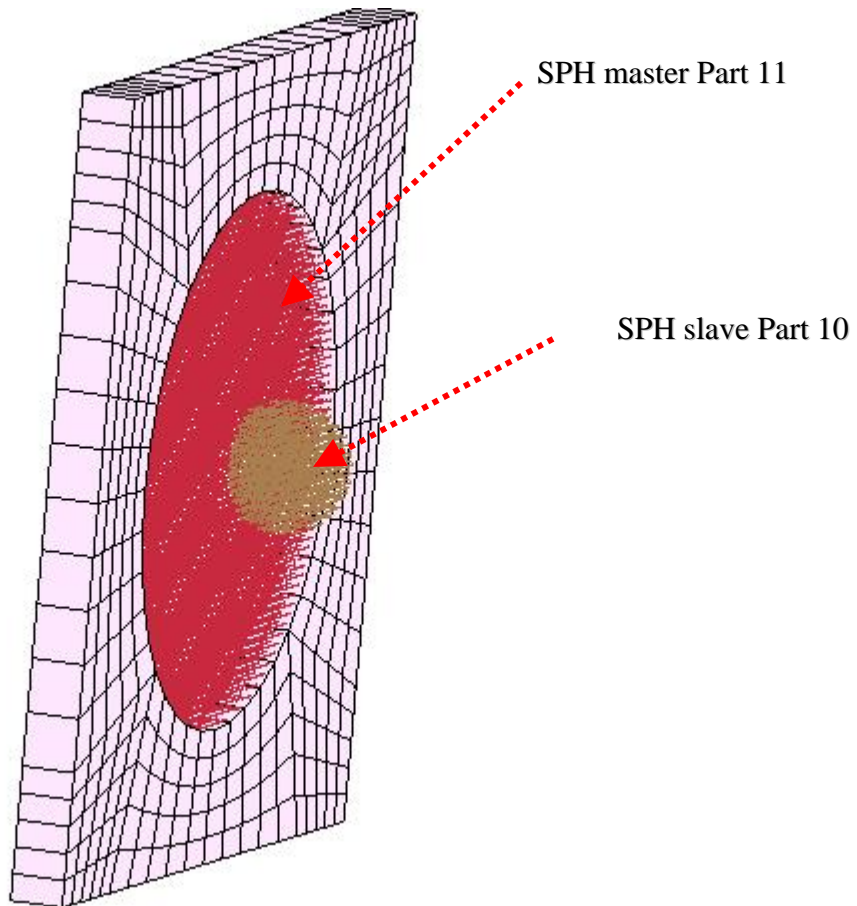
*DEFINE_SPH_TO_SPH_COUPLING

Variables:

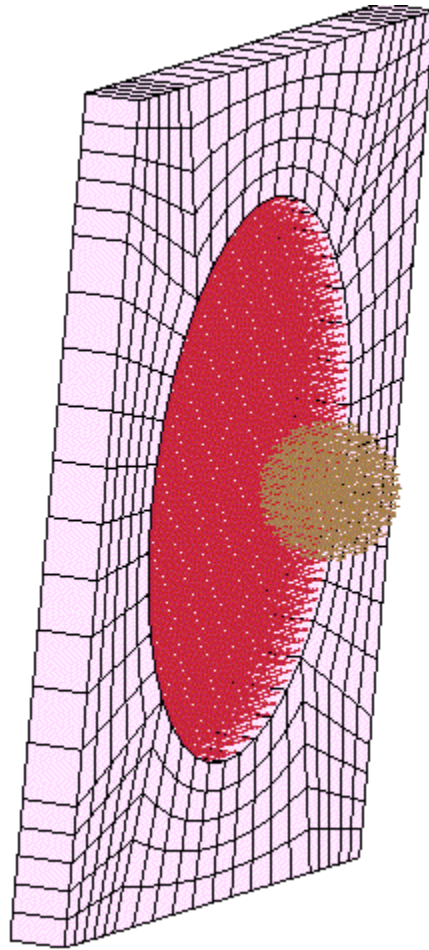
SSID:	Slave part or part set ID
MSID:	Master part or part set ID
SSTYPE	SPH part type: EQ. 0: SSID is part set ID EQ. 1: ISSID is part ID
MSTYPE	SPH part type: EQ. 0: MSID is part set ID EQ. 1: MSID is part ID
IBOX1:	Box ID for slave parts
IBOX2:	Box ID for master parts
PFACT	Penalty scale factor

*DEFINE_SPH_TO_SPH_COUPLING

Used for parts having different densities: gas and water



***DEFINE_SPH_TO_SPH_COUPLING**



SPH Thermal

A new explicit thermal conduction solver is implemented for SPH analysis

Following keywords are supported

- **INITIAL_TEMPERATURE_OPTION*
- **BOUNDARY_TEMPERATURE_OPTION*
- **BOUNDARY_FLUX_OPTION*

Thermal coupling with SPH is implemented

SPH Thermal

```
*CONTROL_SOLUTION
$  soln
   2
```

0=mechanical
1=thermal
2=coupled
(used 2 for SPH thermal)

```
*CONTROL_THERMAL_SOLVER
$  atype  ....  Eqheat  fwork
   1
```

0=steady
1=transient

EQHEAT=mechanical equivalent of heat
conversion factor
FWORK=fraction of mechanical work
converted into heat

```
*CONTROL_THERMAL_TIMESTEP
$  tsc  tip  its
   1  1.0  .1
```

tsc=0 fixed time step
1 variable time step
tip=1.0 full implicit
0.5 Crank Nicolson
tts=0.1 initial time step

*MAT_THERMAL_ISOTROPIC for the part TMID option

SPH Thermal

Conductivity equation for Temperature

$$\rho \cdot C_v \frac{\partial T}{\partial t} = \kappa \frac{\partial^2 T}{\partial x^2}$$

T: temperature

ρ : density

κ thermal conductivity

C_v heat capacity

For SPH thermal equation is solved explicitly
For FEM thermal equation is solved implicitly

FE vs SPH - Pure thermal conduction

Time = 0

Contours of Temperature

min=0, at node# 1

max=100, at node# 3485

Fringe Levels

1.000e+02

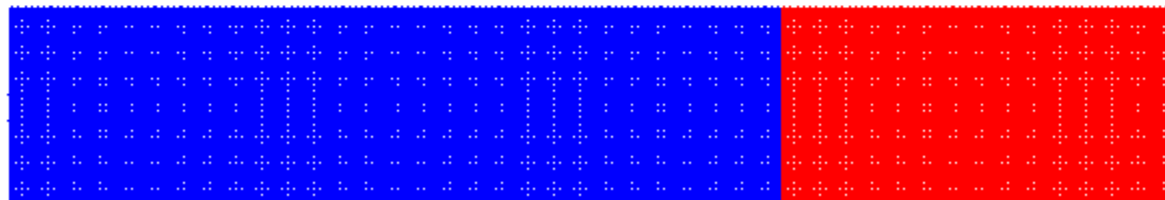
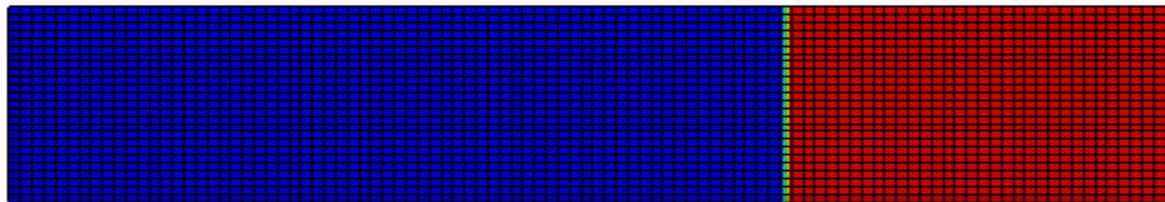
8.000e+01

6.000e+01

4.000e+01

2.000e+01

0.000e+00



Thank you