



Element Sizes in Crash Calculation

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4. LS-DYNA Forum, 20.-21. Oktober 2005, Bamberg


Investigation on mesh density in LS Dyna **TECOSIM**

Agenda


- Tecosim-best partner for simulation
- Introduction
- FE Experiments with varied parameters
- Analysis of Results/ Conclusion
- Outlook

Locations & References






Rüsselsheim




Köln

- Audi AG
- Adam OPEL AG
- Claas
- Daimler Chrysler
- Daihatsu
- Fiat
- FORD
- General Motors
- HONDA
- ISUZU
- KIA
- John Deere
- Jaguar
- Landrover
- Nissan
- PORSCHE AG
- Toyota


- AMG
- Autoliv
- Bayer AG
- Bentler
- Bertone
- Bosch/ Blaupunkt
- Degussa-Hüls AG
- Dynamit Nobel
- EADS
- Faurecia
- Getrag
- Hella KG
- Johnson Controls
- Karmann
- Lear
- Magna
- Thyssenkrupp
- TRW Automotive
- Mahle
- MAN
- Mannesmann/Sachs
- Siemens VDO
- Wagon Automotive




Leonberg



Basildon (UK)



Coventry (UK)



Igenie Office
Tokio (Japan)

CAE Portfolio





CRASH



Safety



NVH / Durability



Powertrain



Seats

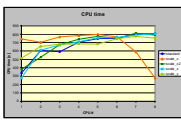
CAE Portfolio



Multi Body Systems (MBS)



CFD



Optimization



Software dev

Introduction



***Any sufficiently advanced
technology is indistinguishable
from magic.***

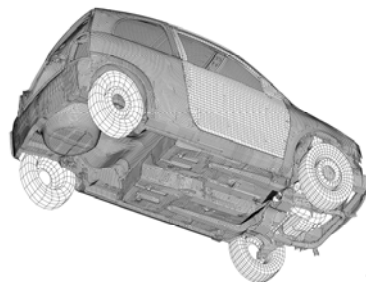
„Profiles of the future“ (1961) by Arthur C. Clarke (2003)

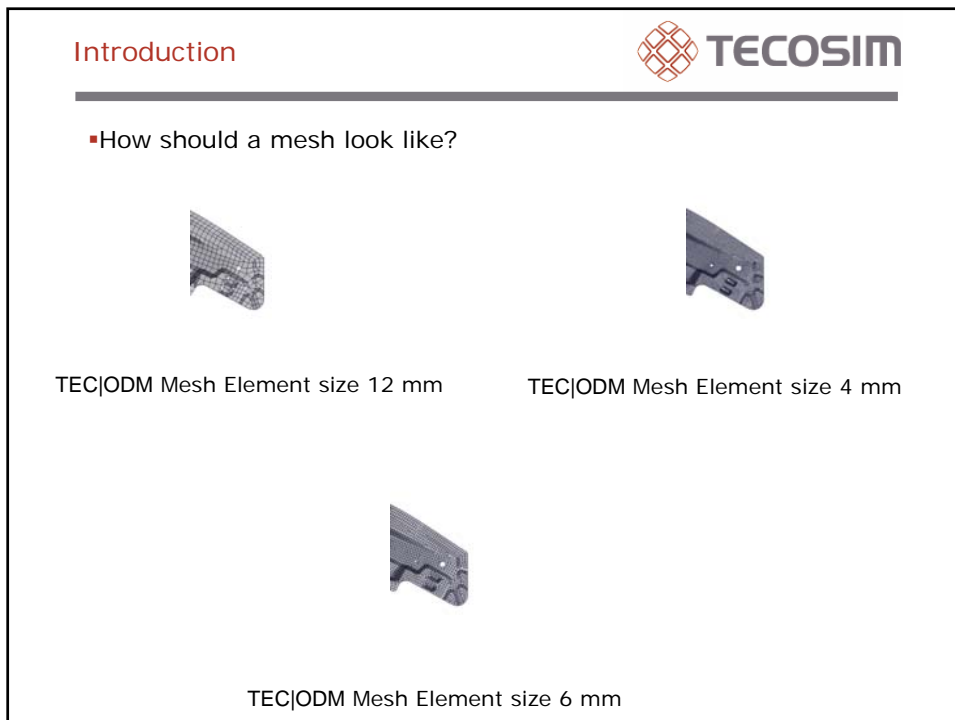
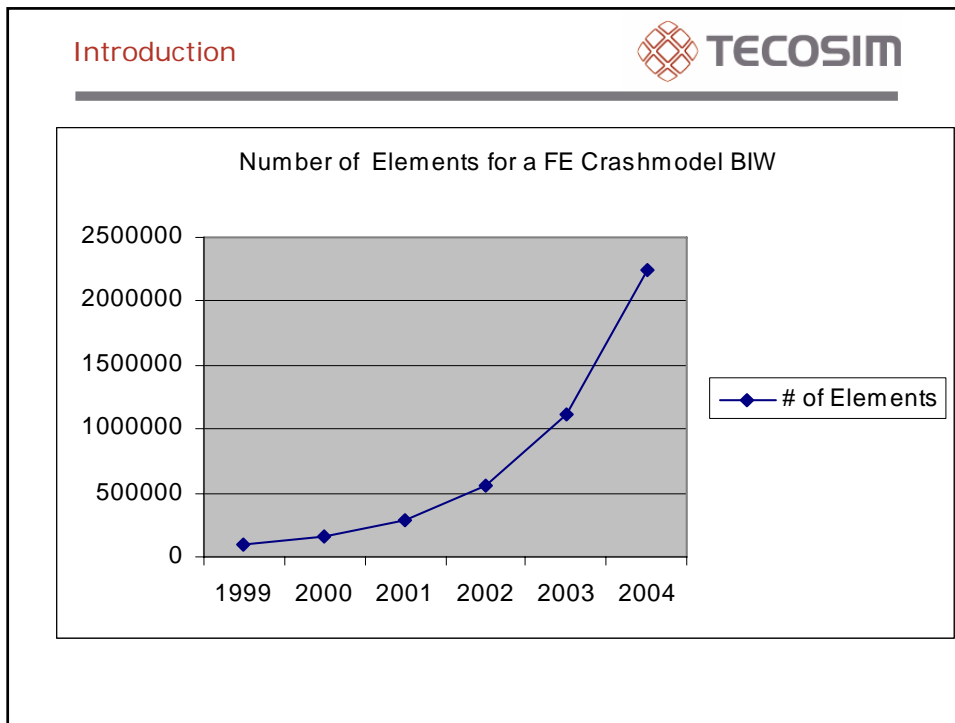
Introduction



- Why do we simulate?
- Cost effective
- Fast
- Proven method

- *We cannot test!*





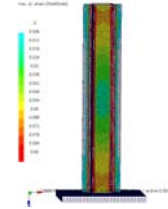
FE Experiments with varied parameters

**Simple box crash experiment:**

Box section 50 mm x 80 x 500mm, t= 1.0mm, mild steel

Varied parameters:

- average edge length 15/10/5/2,5mm
- mesh orientation 0deg/ 25deg
- different mesh/ integration method: Belytschko-Tsay/ Fully Integration
- Varied number of spotwelds
- With and without mapping or stamping data
- Renumbering and move in space



Objective:

- Is the result depending on the element length?
- Is the result depending on the element orientation?
- How does mapping influence/stabilise the results?
- How do small changes in the input influence the results?

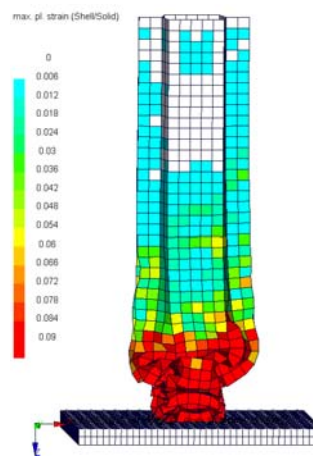
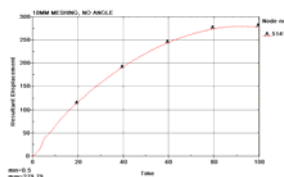
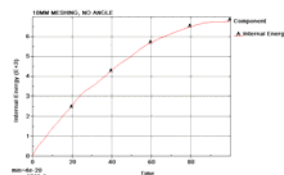
FE Experiments with varied parameters

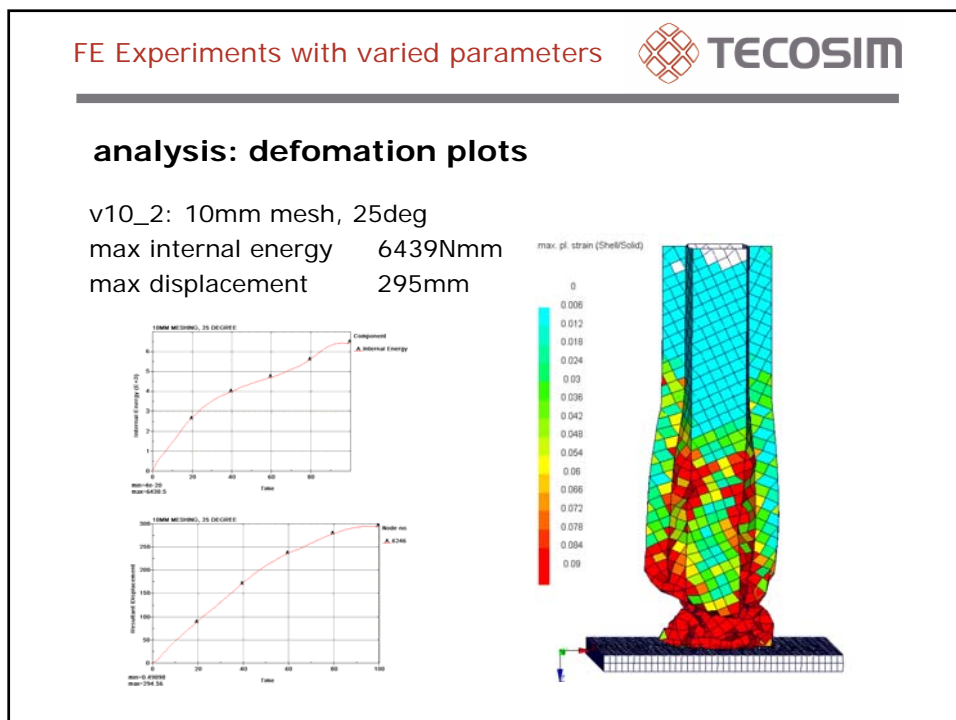
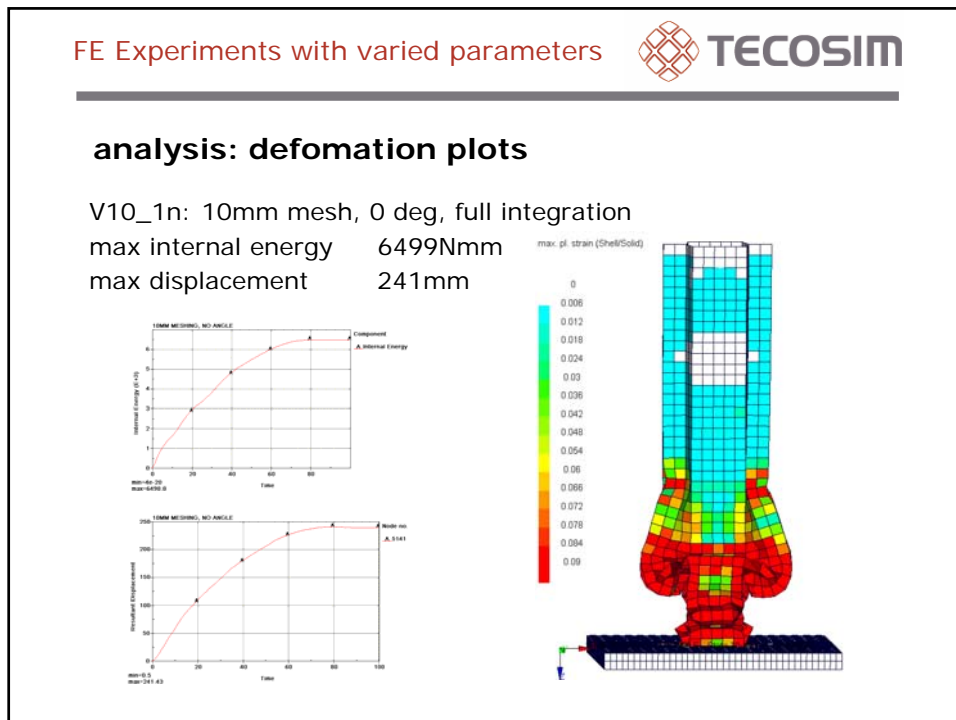
**analysis: defomation plots**

v10_1: 10mm mesh, 0deg

max internal energy 6766Nmm

max displacement 278mm



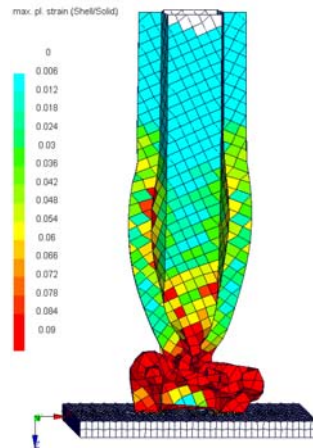
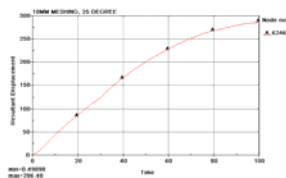
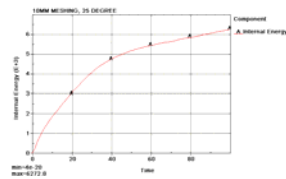


FE Experiments with varied parameters



analysis: defomation plots

V10_2n: 10mm mesh, 25 deg, full integration
 max internal energy 6272Nmm
 max displacement 286mm

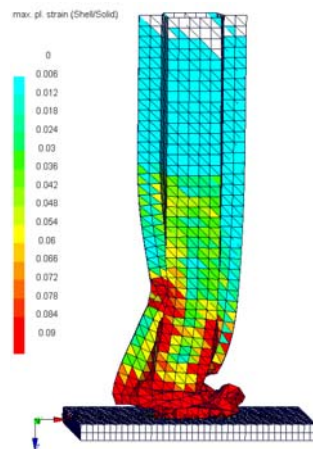
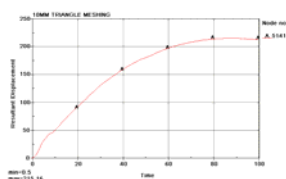
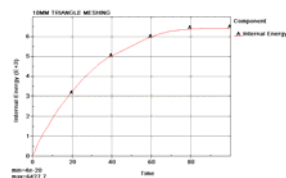


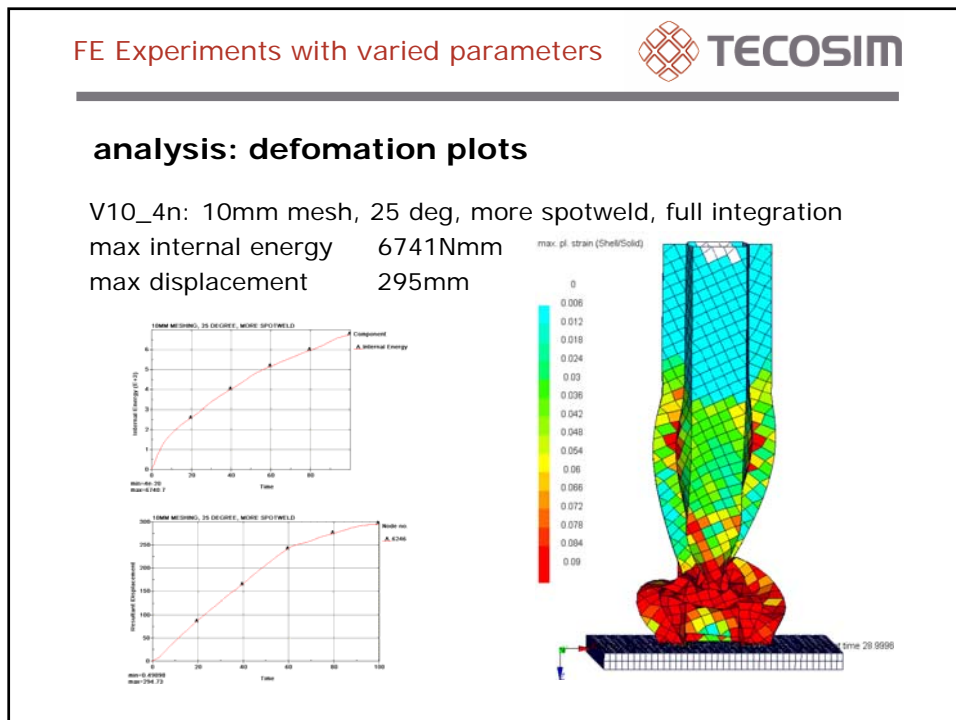
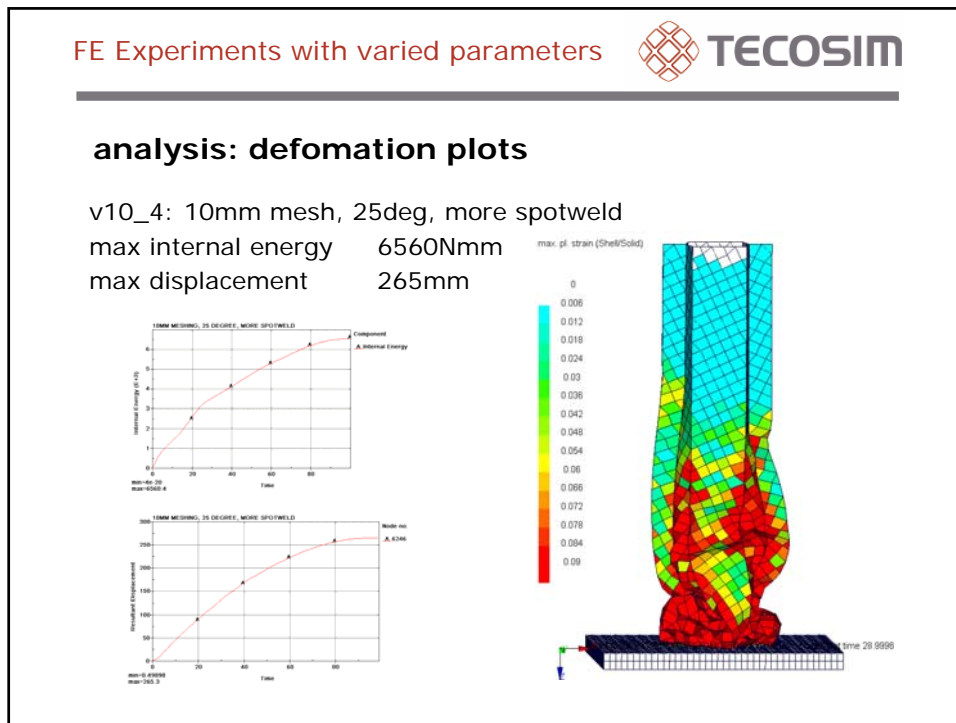
FE Experiments with varied parameters

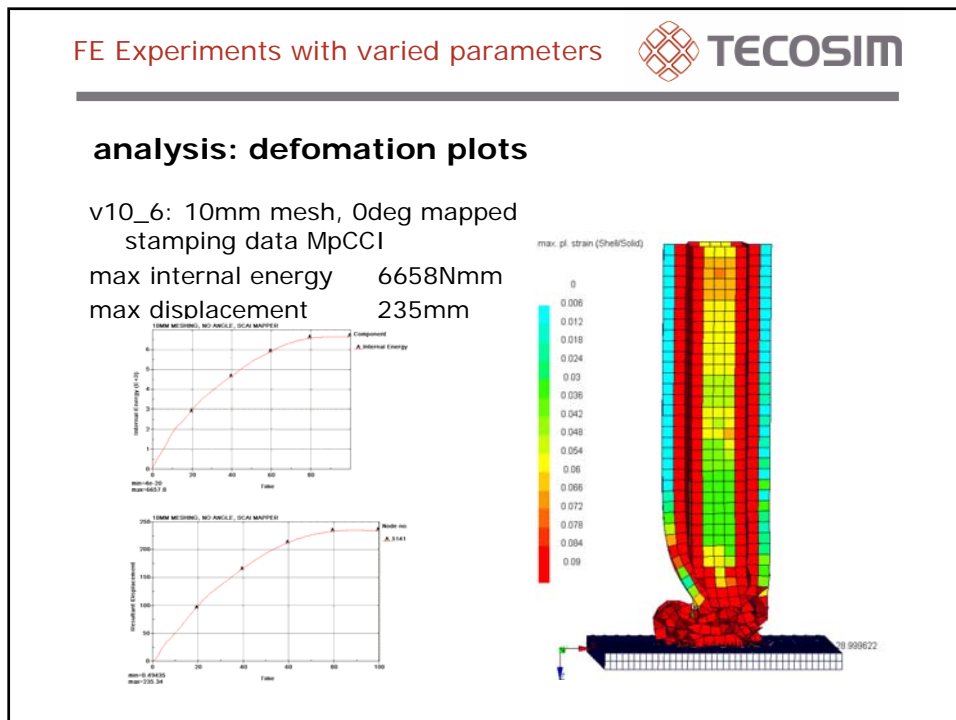
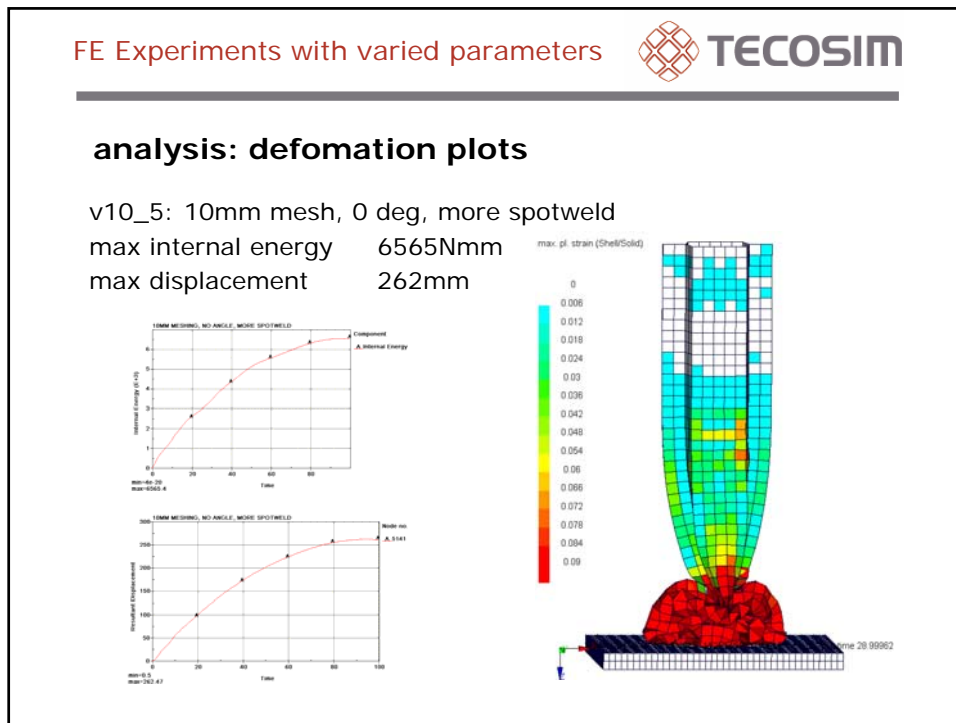


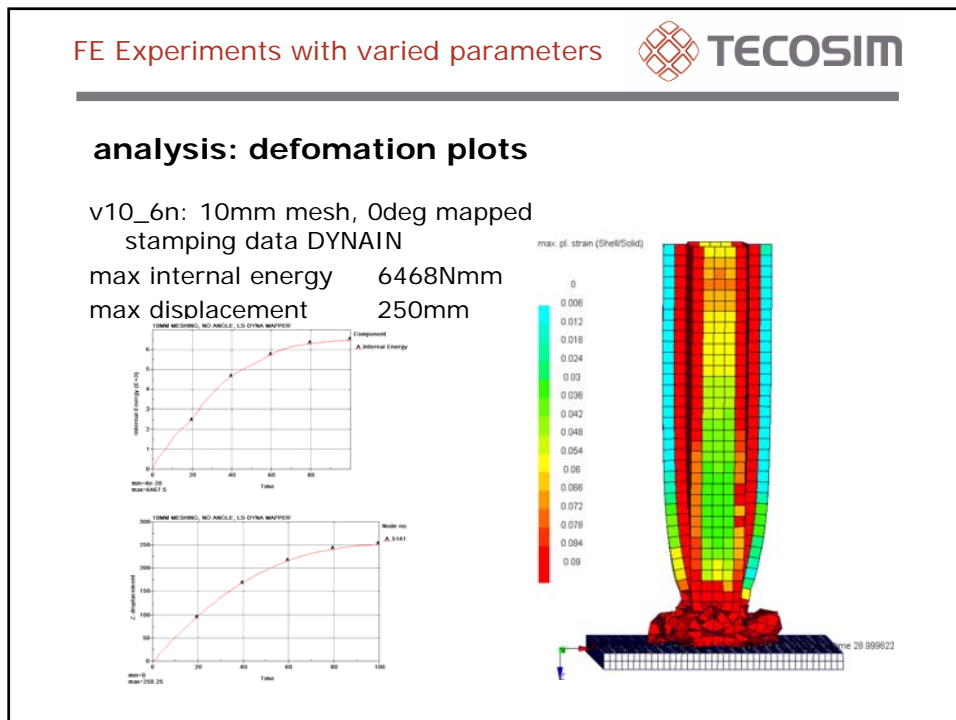
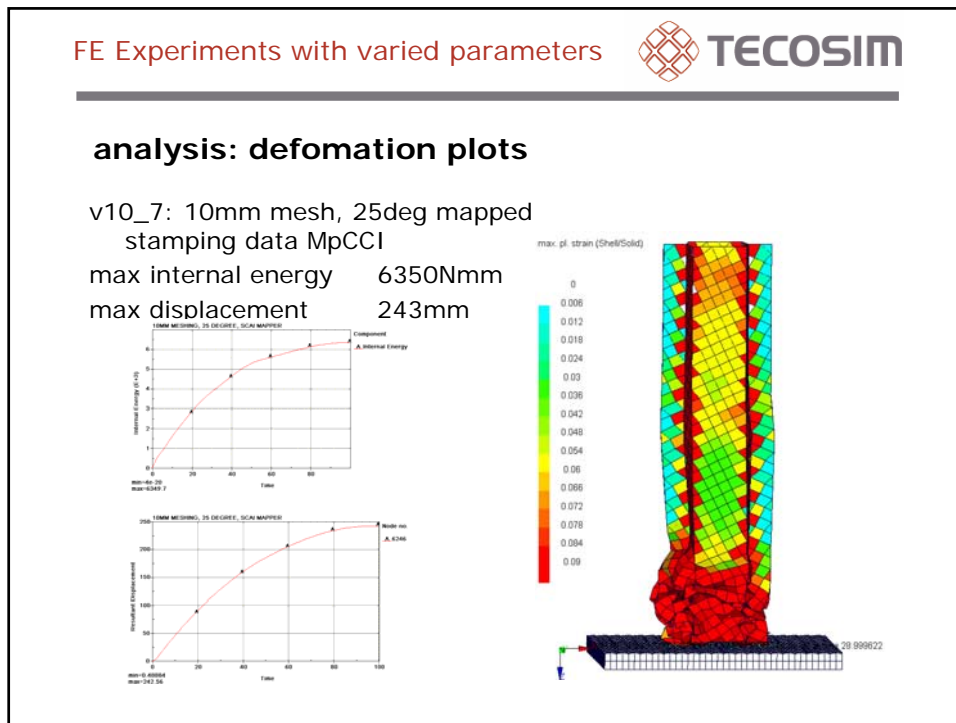
analysis: defomation plots

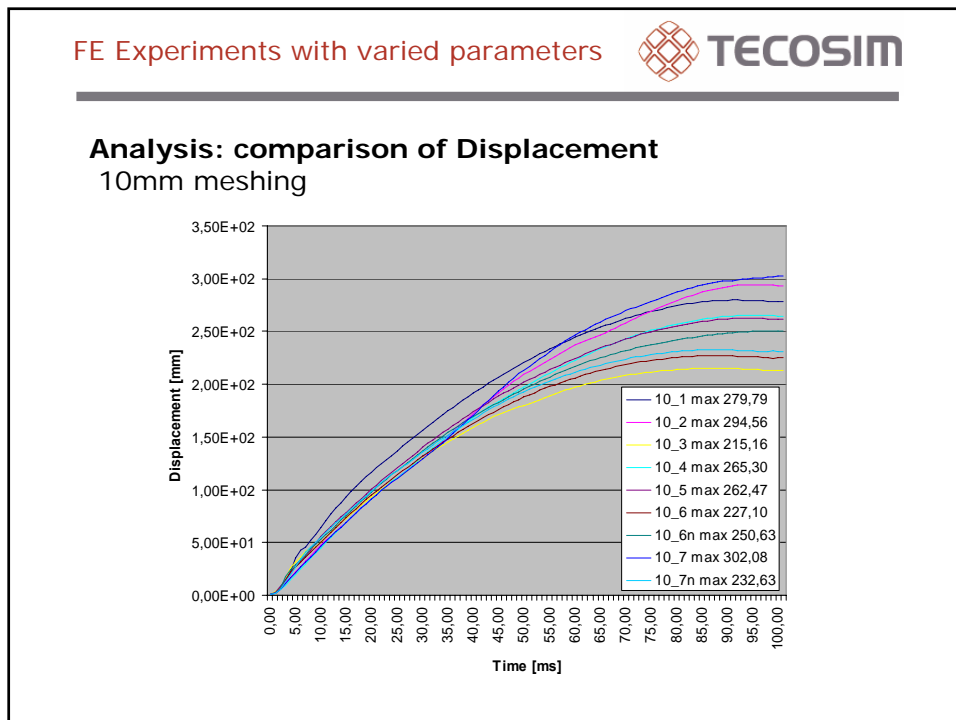
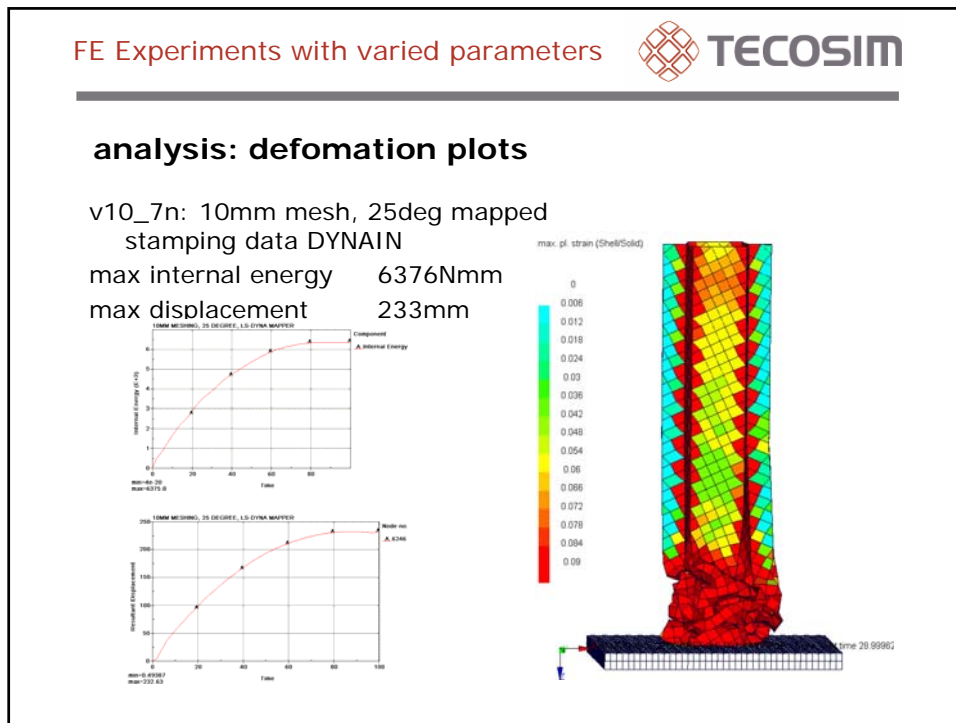
v10_3: 10mm triangle mesh
 max internal energy 6428Nmm
 max displacement 215mm

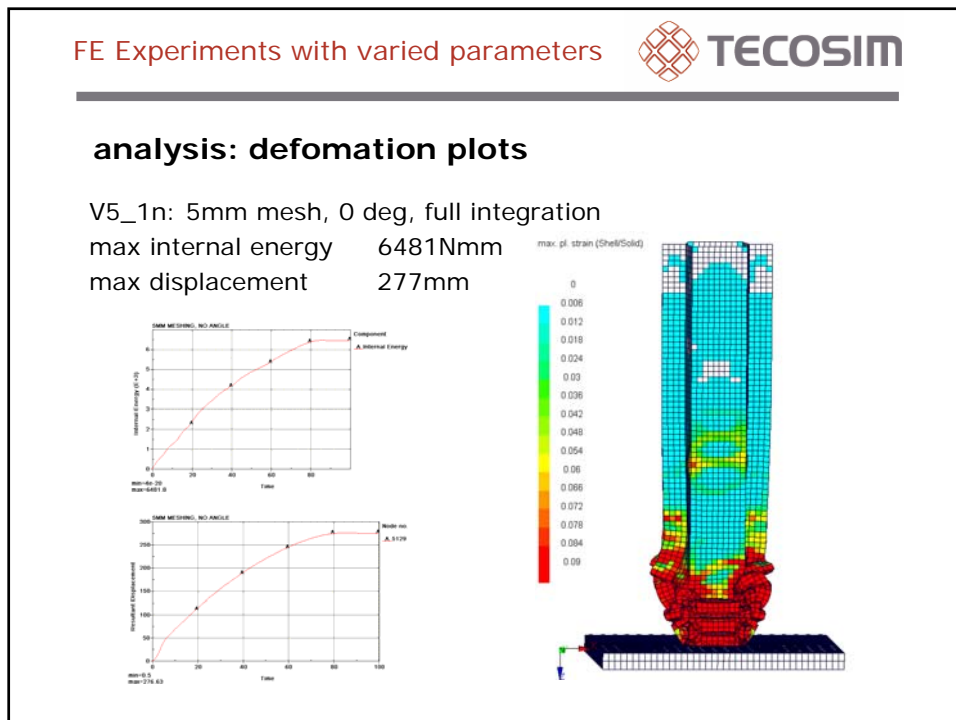
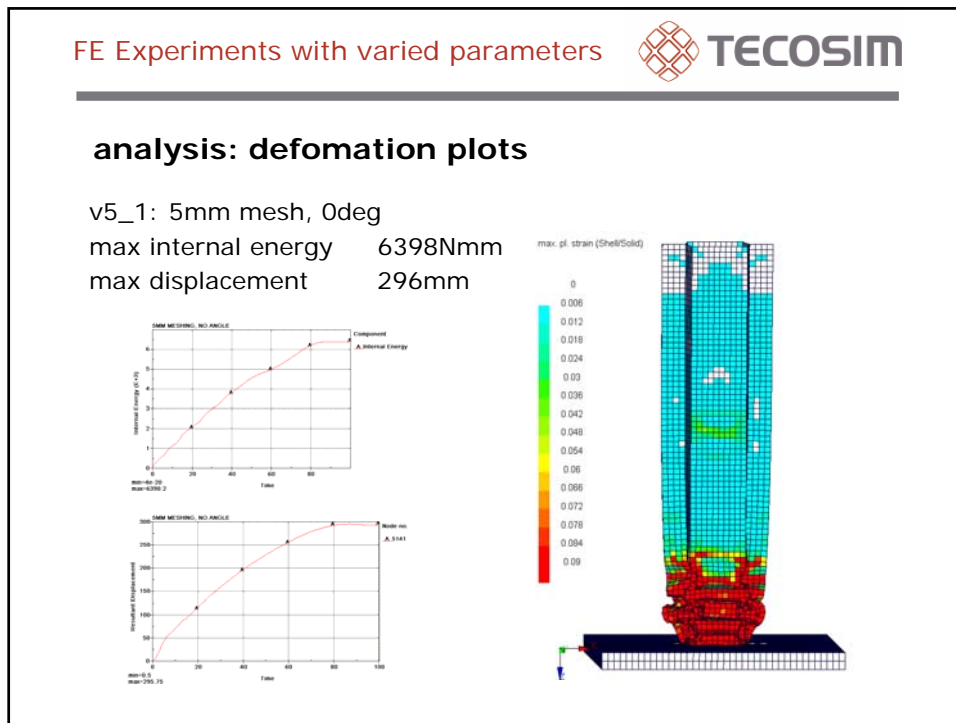










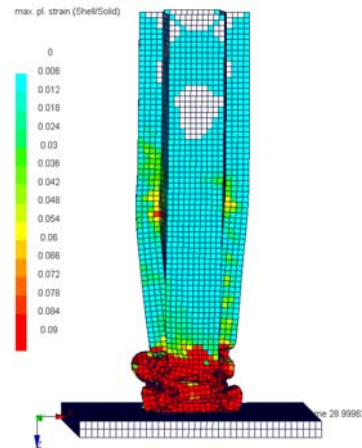
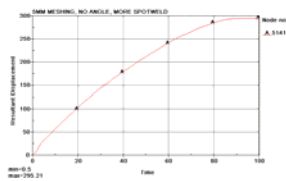
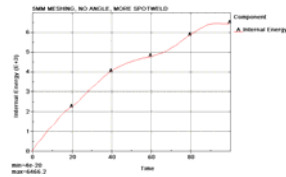


FE Experiments with varied parameters



analysis: defomation plots

v5_5: 5 mm mesh, 0 deg, more spotweld
 max internal energy 6466Nmm
 max displacement 295mm

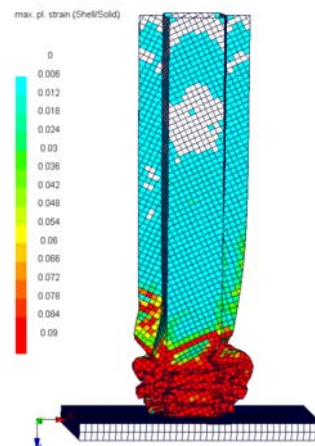
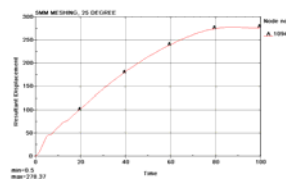
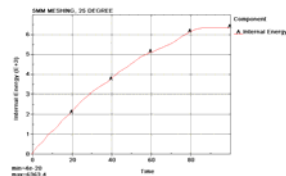


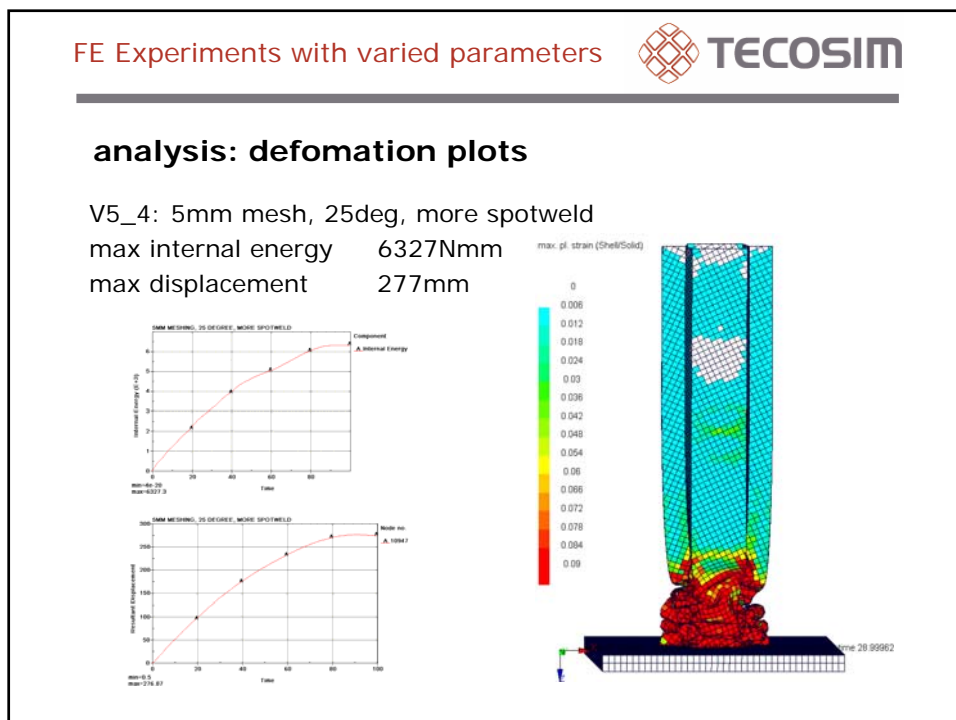
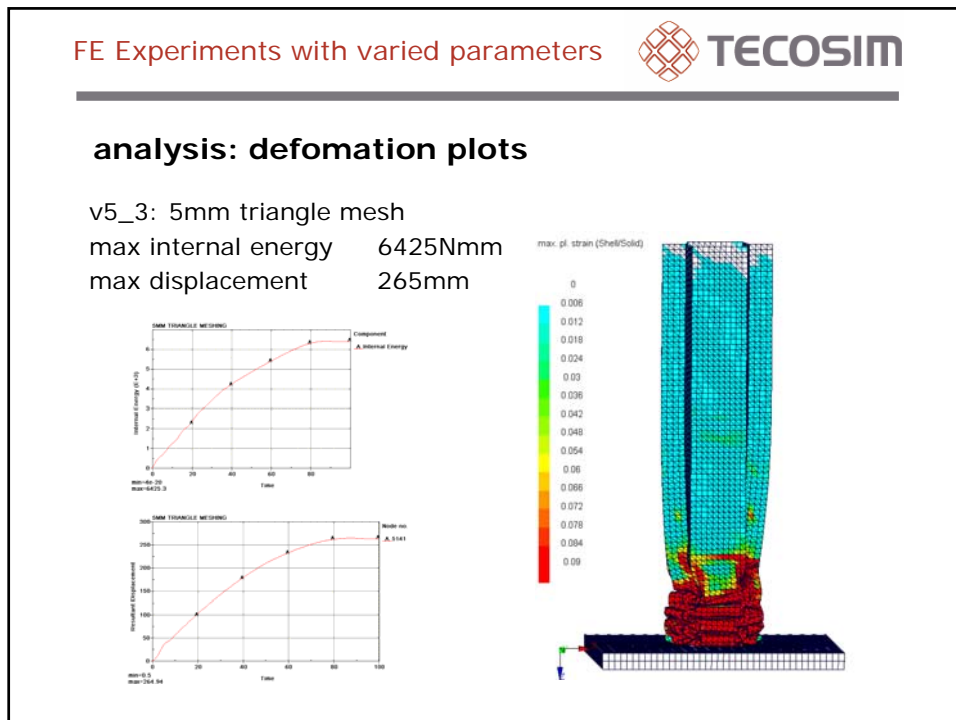
FE Experiments with varied parameters



analysis: defomation plots

v5_2: 5mm mesh, 25deg
 max internal energy 6363Nmm
 max displacement 278mm



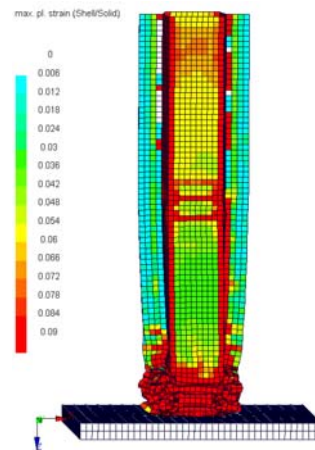
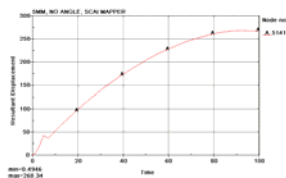
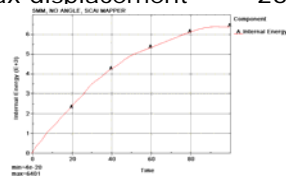


FE Experiments with varied parameters



analysis: defomation plots

v5_6: 5mm mesh, 0deg mapped
 stamping data MpCCI
 max internal energy 6401Nmm
 max displacement 268mm

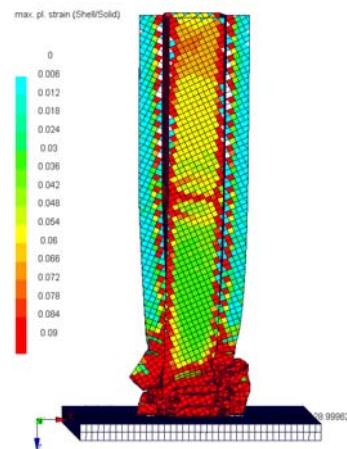
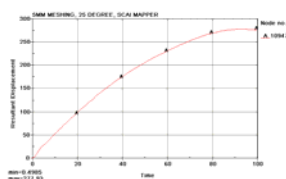
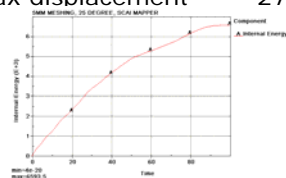


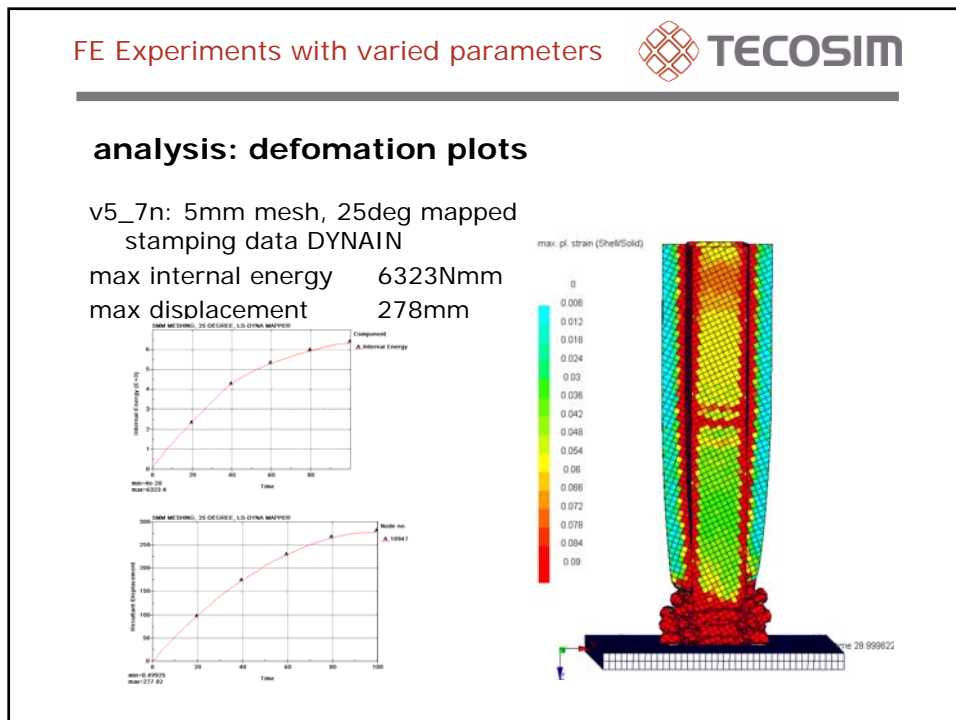
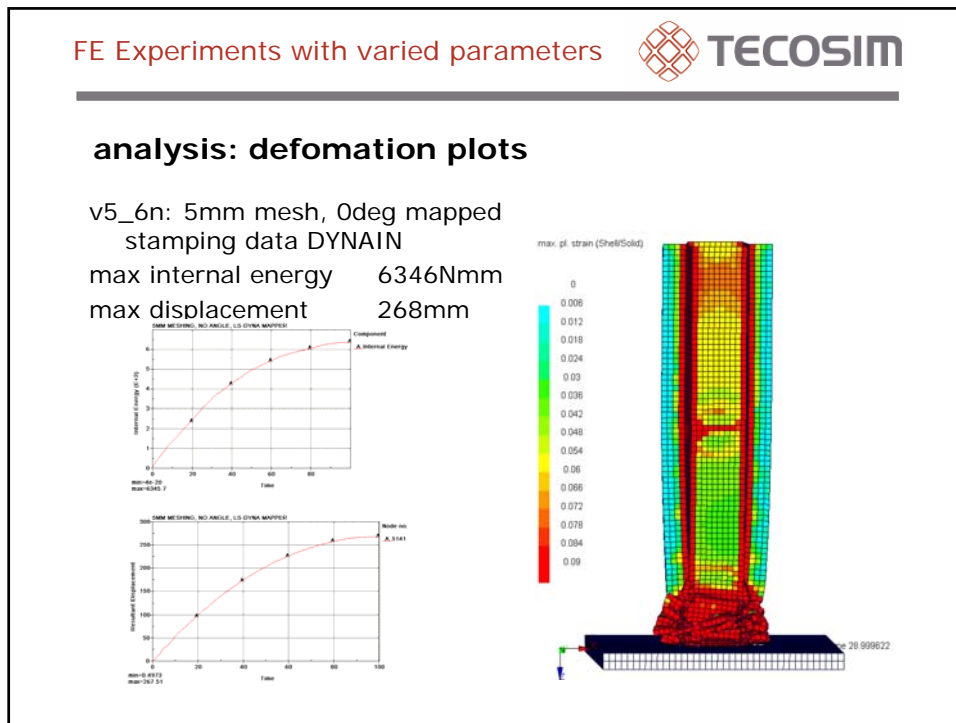
FE Experiments with varied parameters

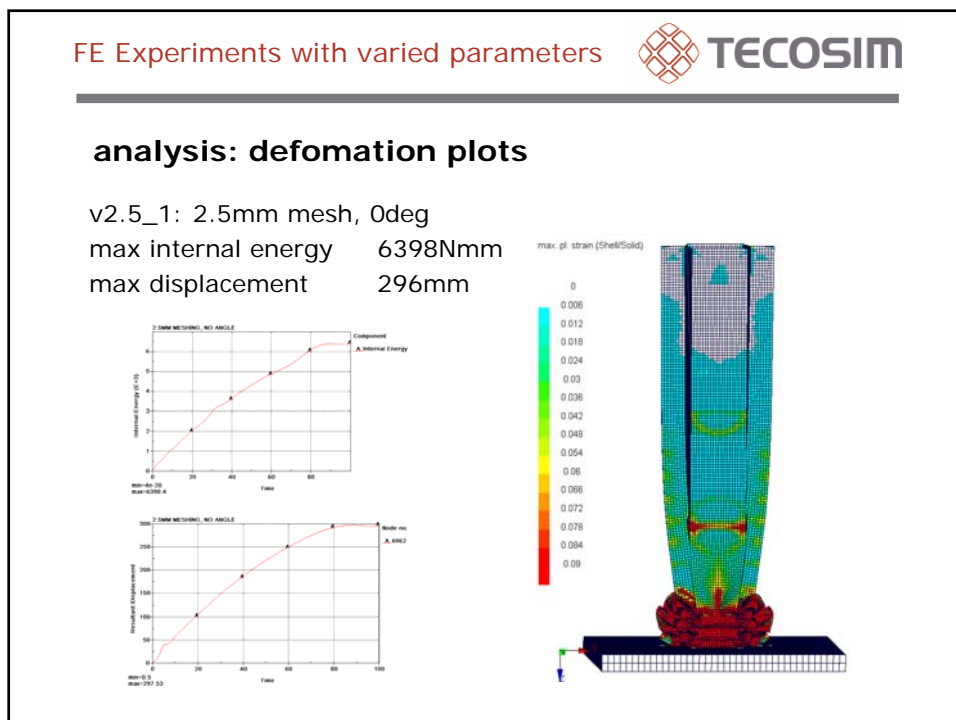
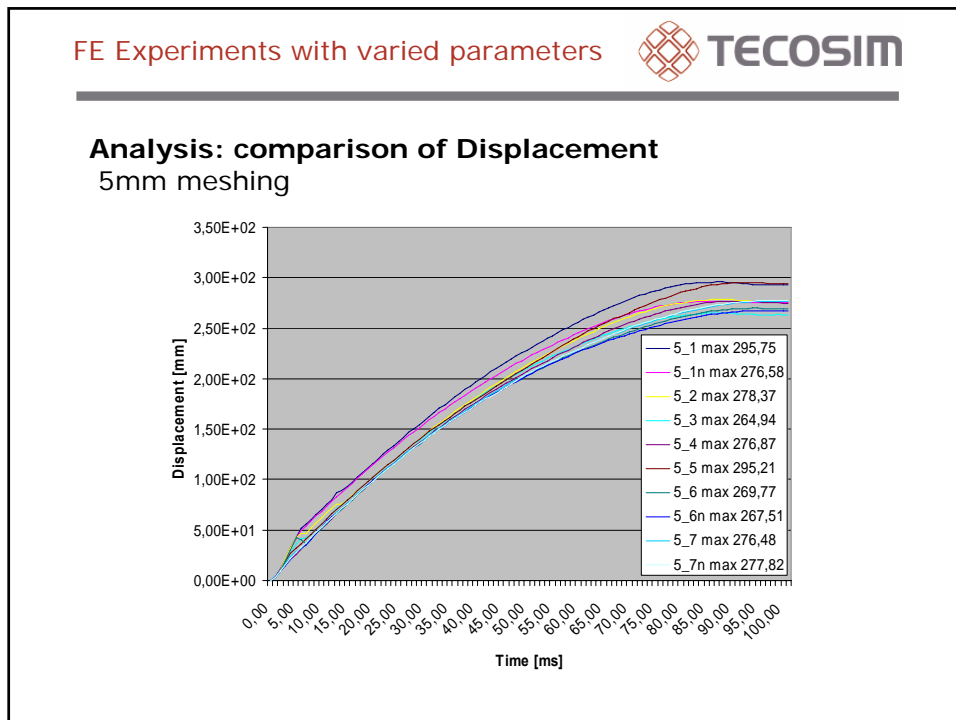


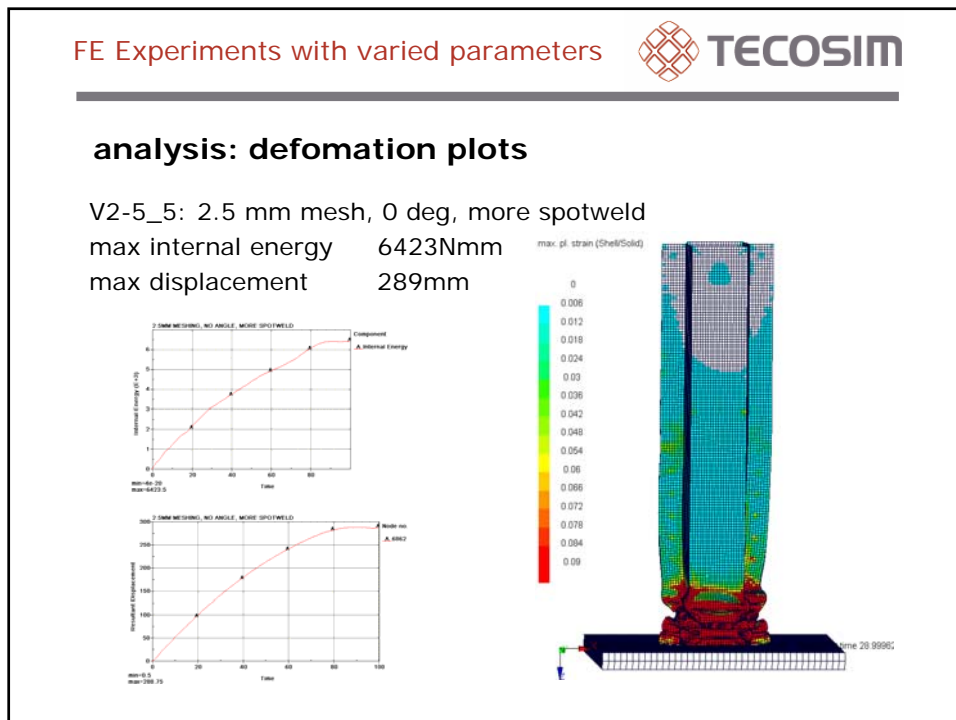
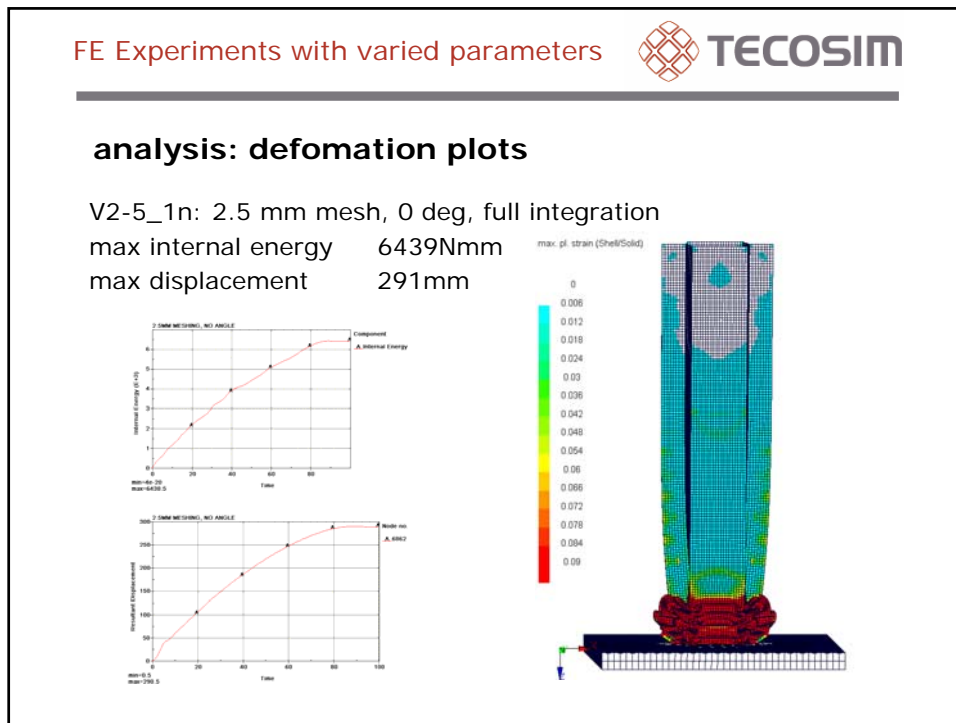
analysis: defomation plots

v5_7: 5mm mesh, 25deg mapped
 stamping data MpCCI
 max internal energy 6593Nmm
 max displacement 278mm







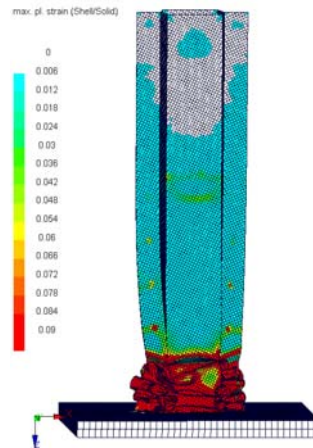
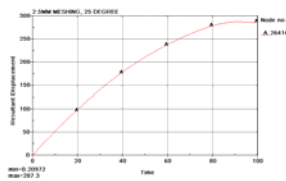
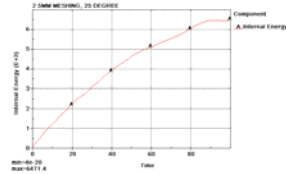


FE Experiments with varied parameters



analysis: defomation plots

V2-5_2n: 2.5 mm mesh, 25 deg
 max internal energy 6471Nmm
 max displacement 287mm

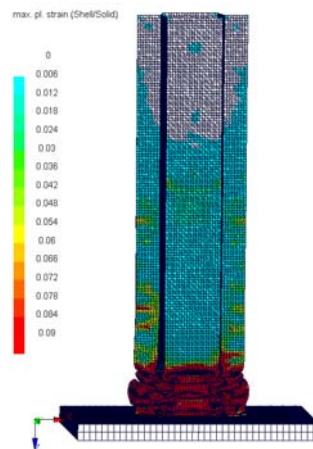
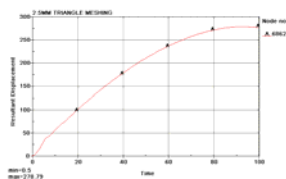
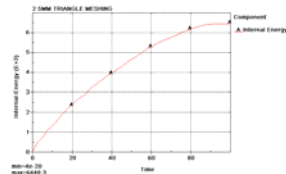


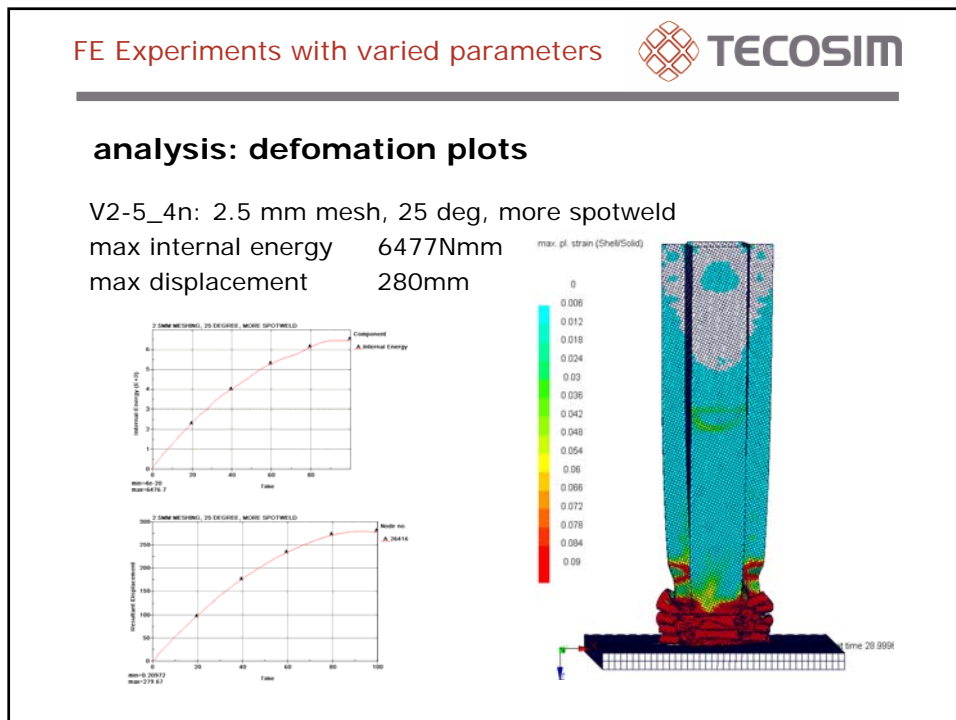
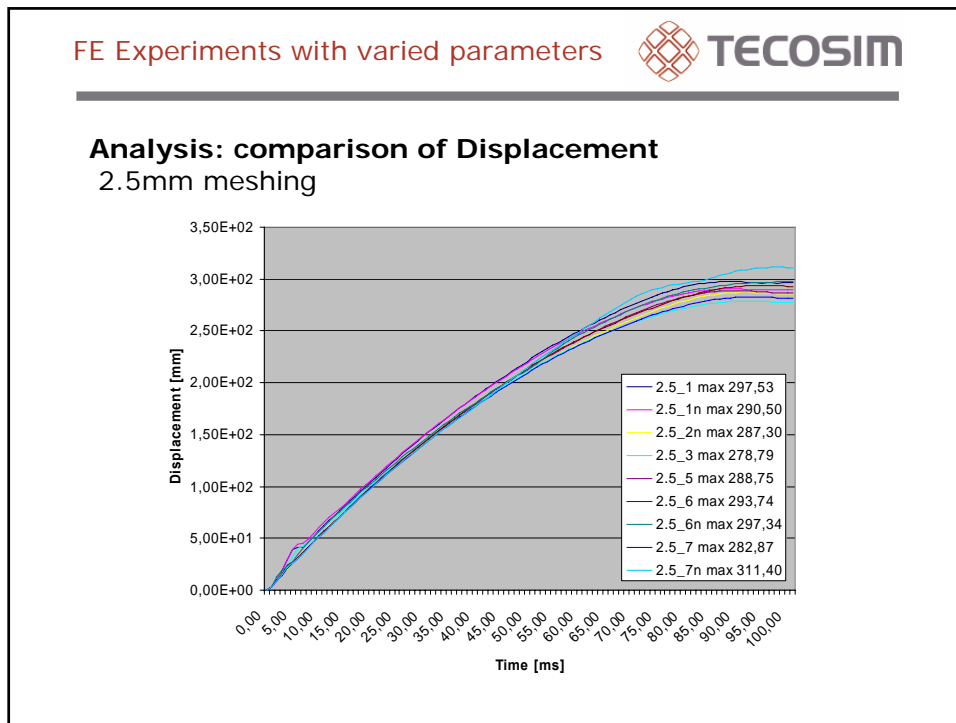
FE Experiments with varied parameters

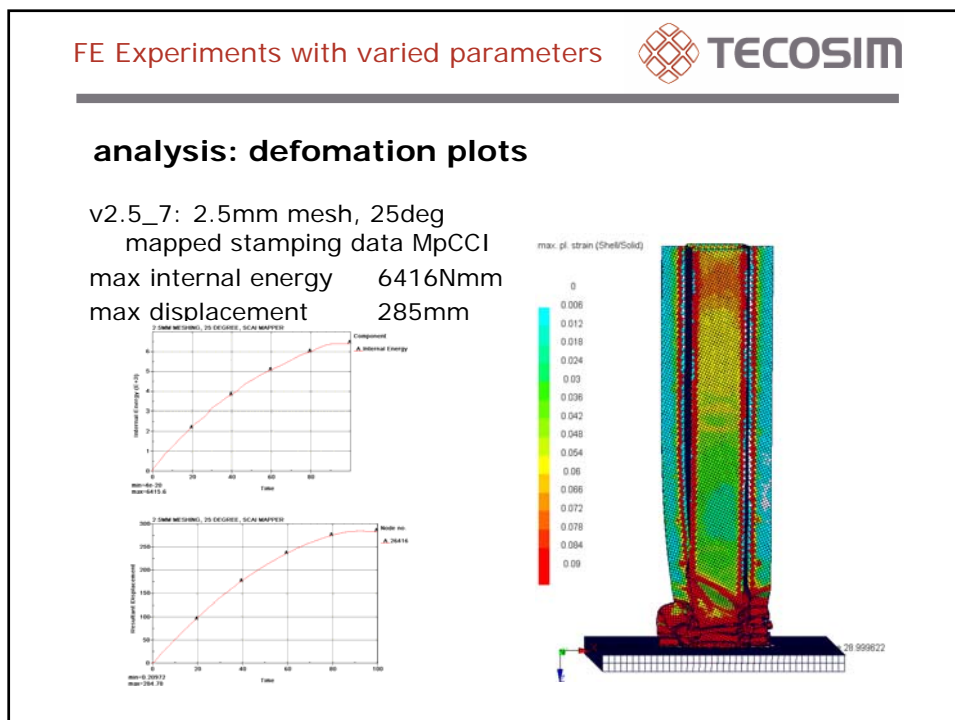
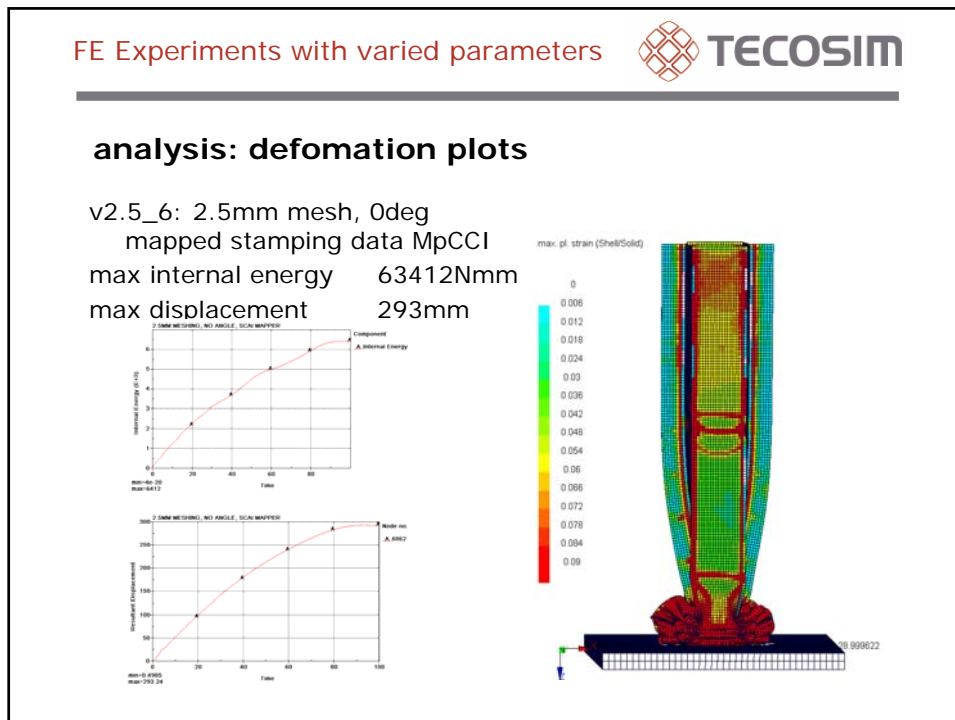


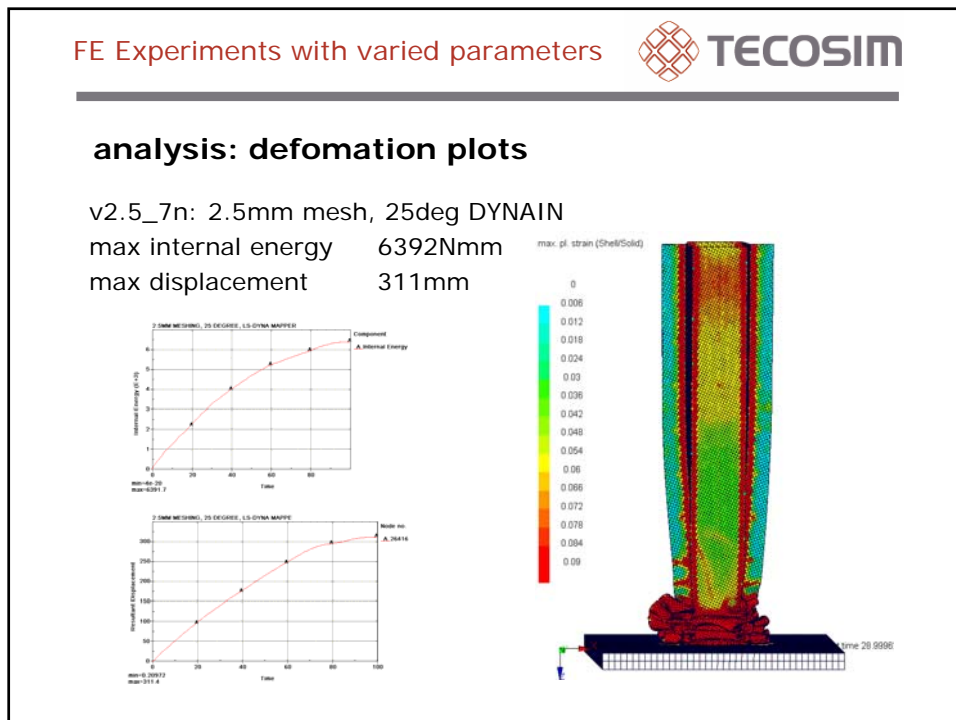
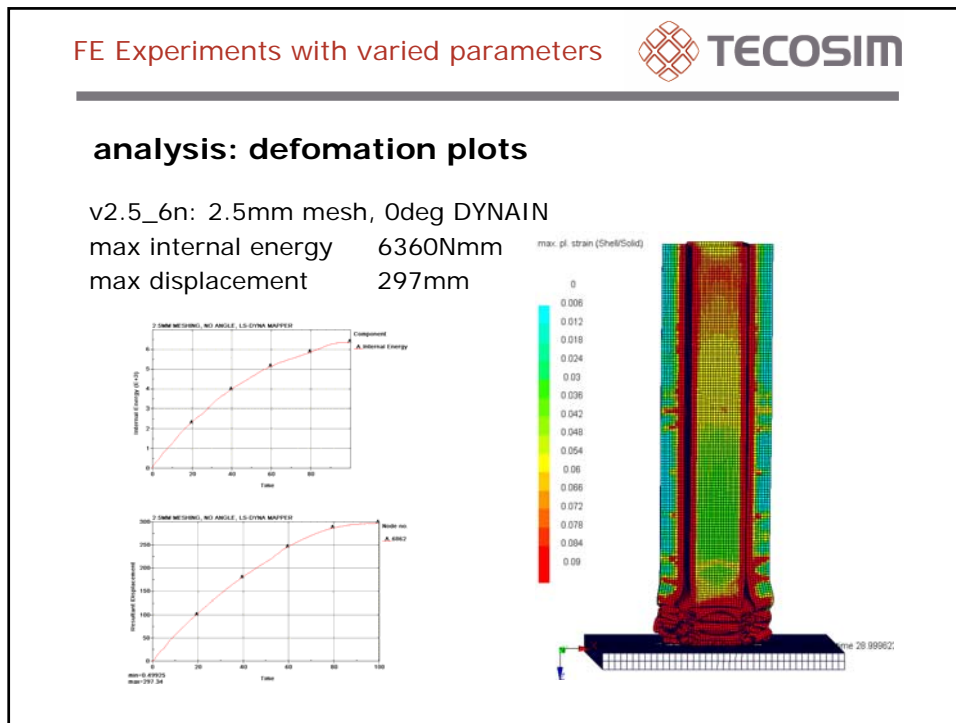
analysis: defomation plots

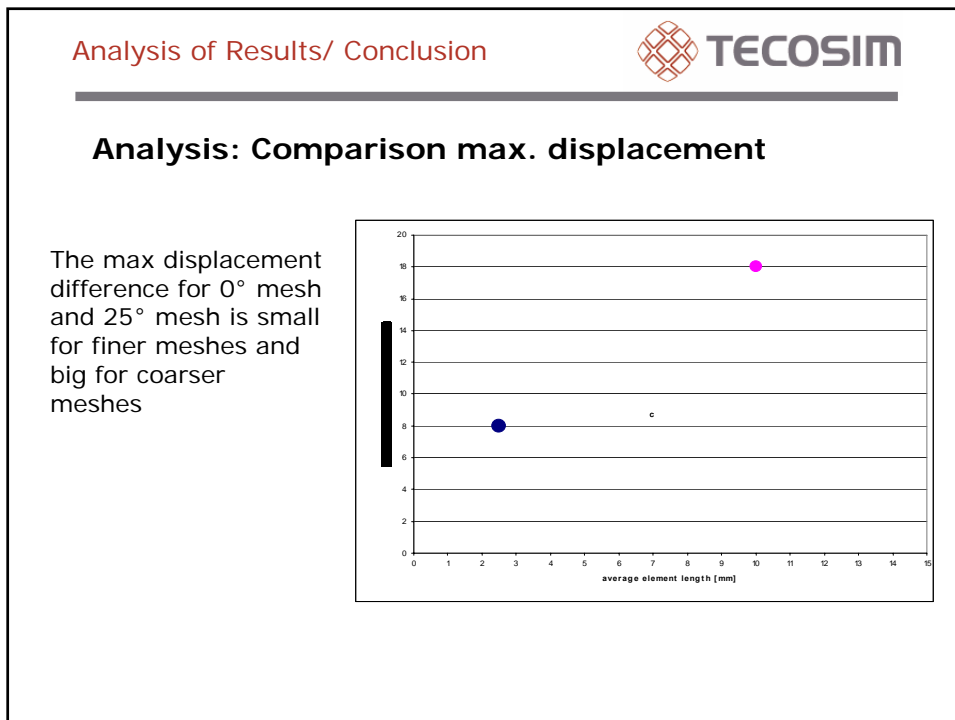
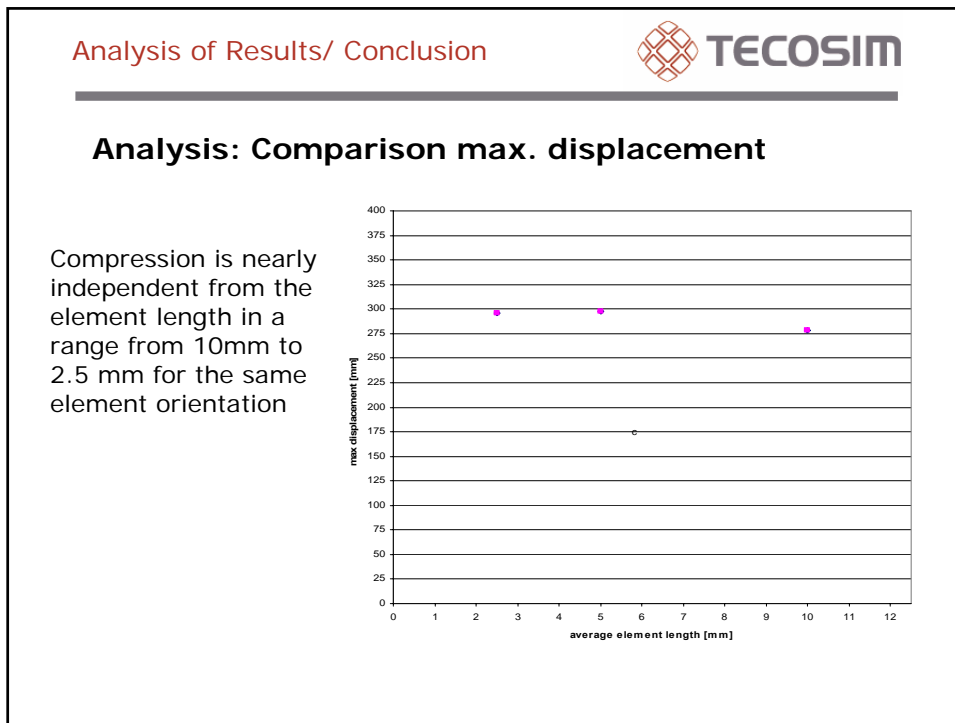
v2.5_3: 2.5mm triangle mesh
 max internal energy 6448Nmm
 max displacement 279mm

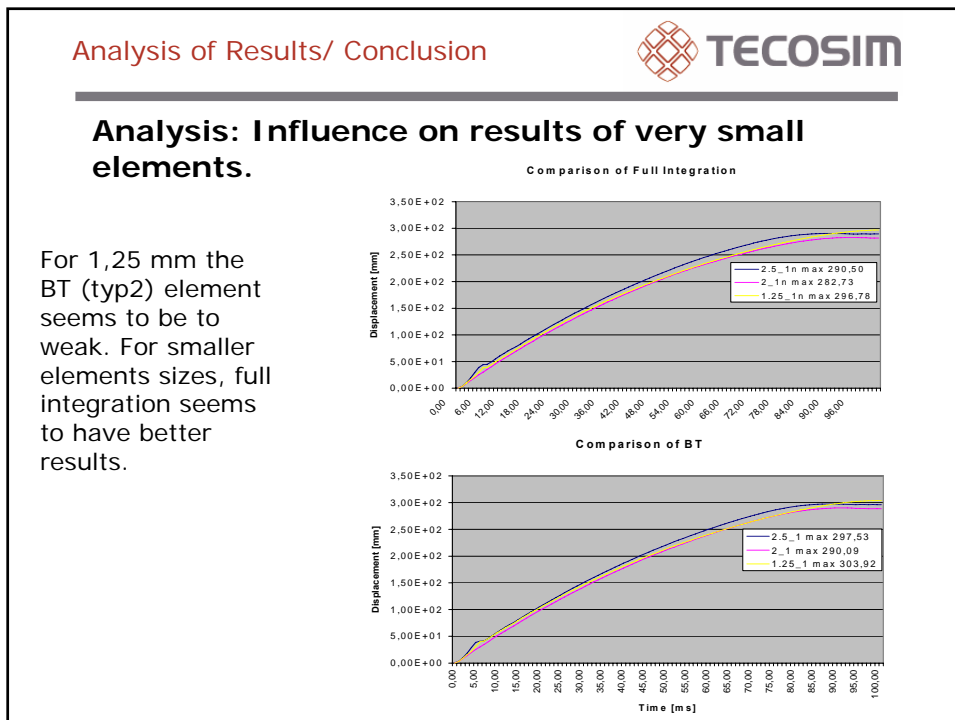
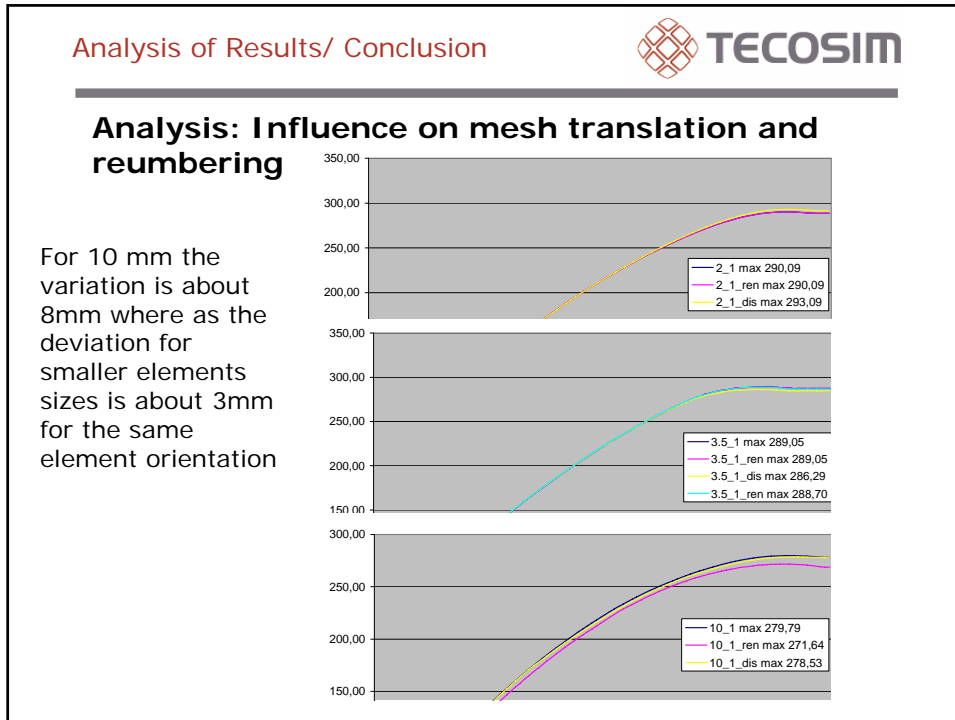


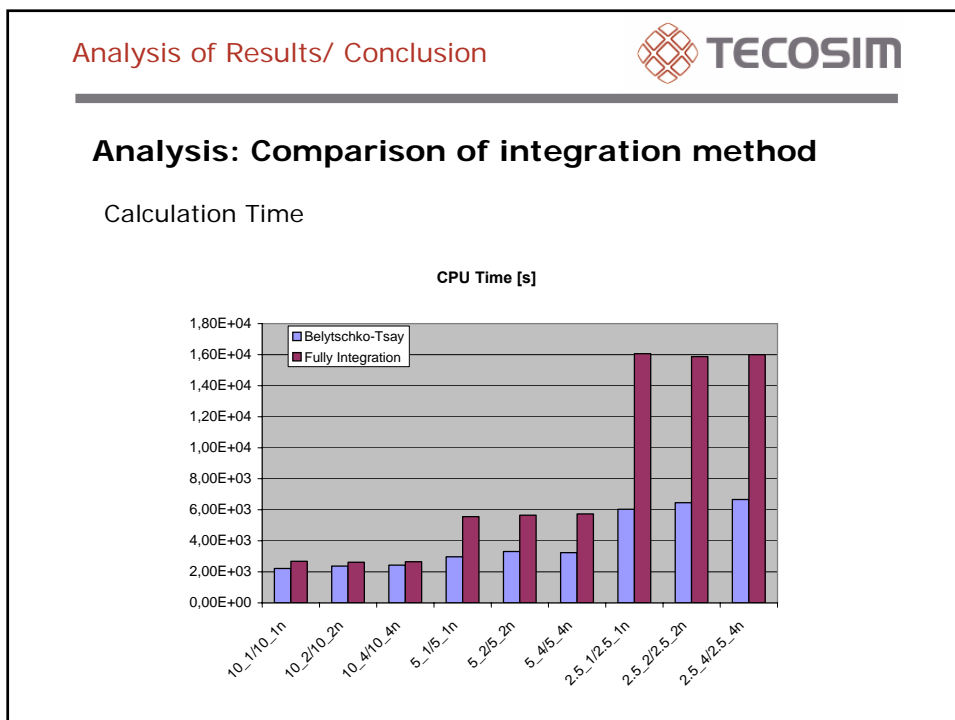
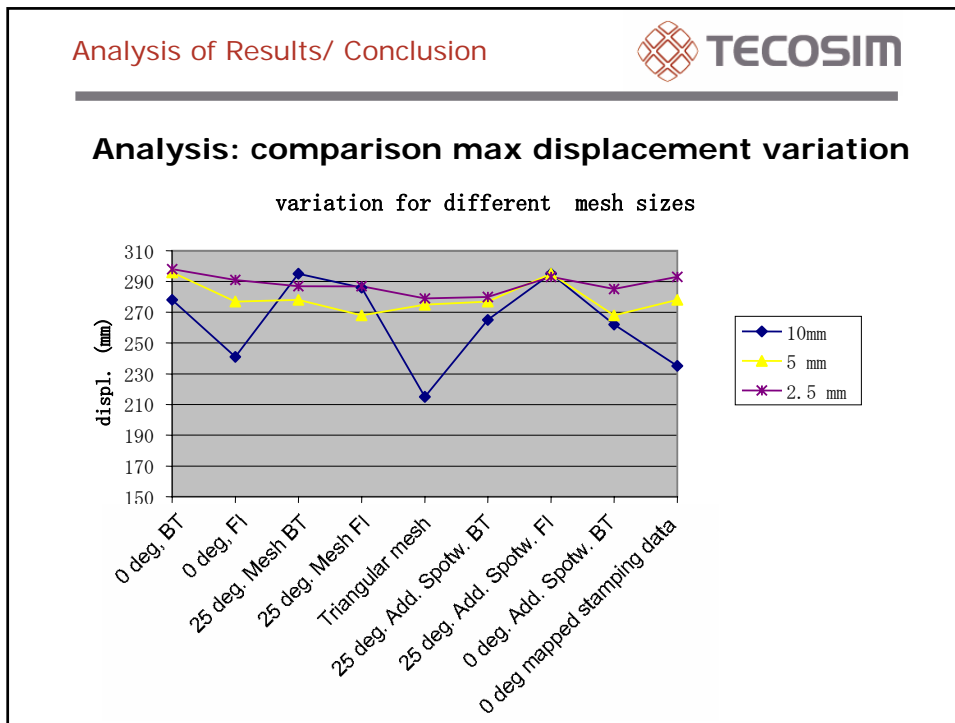












Analysis of Results/ Conclusion

**Results**

- Results for the displacement and the internal energy seem to be smooth and stable in a range from 15mm to 2,5 mm for orthogonal element orientation
- Different element orientation give different results for coarser meshes
- Finer mesh is not so sensitive for different element orientation, integration method, number of spotwelds, mapping, small changes in the input (renumbering, moving the model in space)
- Mapping tools are easy to use for Crash coupling. The influence of the mapping was getting smaller for smaller element sizes for the influenced zone was getting smaller and the crash mode was very stable in our example.

Analysis of Results/ Conclusion

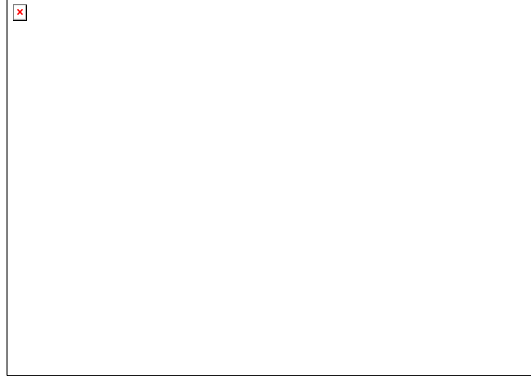
**Conclusion**

- If you know the collapse mode of a part you can use a coarse mesh which should be orthogonal in the collapse direction (so you can achieve "superconvergence")
 - If you doesn't know the collapse mode of a part; Please use finer meshes
 - No one knows the exact collapse mode of all the parts in a vehicle!
 - Meshing rules for orthogonal /Mapping/Integration schemes meshes are important for coarser meshes but not important for finer meshes.
-
- *Creation of finer meshes can be automated by TEC|ODM!*

Analysis of Results/ Outlook

**Outlook**

The crashbox sample will be applied to a complete vehicle to find out about the time saving potential and the influence on the results.



Thank you for your attention!
Please ask some questions

